

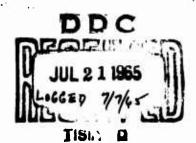
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U. S. A R M Y TRANSPORTATION RESEARCH COMMAND FORT EUSTIS, VIRGINIA

TREC TECHNICAL REPORT 50-53

TWO-DIMENSIONAL WIND-TUNNEL TESTS

of an H-34

MAIN ROTOR AIRFOIL SECTION

Project 9R38-11-009-04

Contract DA 44-177-TC-657

September 1960

prepared by :

United Aircraft Corporation Sikorsky Aircraft Division Stratford, Connecticut





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©TWO-DIMENSIONAL WIND TUNNEL TESTS OF AN H-34 MAIN ROTOR AIRFOIL SECTION.

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UNITED AIRCRAFT CORPORATION SIKORSKY AIRCRAFT DIVISION

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LIST OF SYMBOLS

c	Airfoil chord, feet
pl	Static pressure measured on airfoil lower surface, psf
P _O	Free stream static pressure
$\mathbf{p}_{\mathbf{u}}$	Static pressure measured on airfoil upper surface, psf
q _o	Dynamic pressure 1/2 p V ²
x	Chordwise distance from leading edge, feet
c_D	Section drag coefficient, D/QoS
c_L	Section lift coefficient, L/qoS
c_{L}	Approximate section lift coefficient, $C_N \cos \alpha$
C _m	Section pitching moment coefficient, $M_c/4/q_oSc$
c_N	Normal force coefficient, $C_N = \int_{-\infty}^{c} -(C_{pu} - C_{pl}) d(x/c)$
C _{pu}	Pressure coefficient, upper surface, (pu-po)/qo
Cpl	Pressure coefficient, lower surface, (pl-po)/qo
D	Drag, pounds
L	Lift, pounds
$M_{\rm C}/4$	Pitching moment about quarter chord line, foot-pounds
S	Airfoil plan area, square feet
v	Wind tunnel velocity, fps
a	Corrected angle of attack, degrees
P	Density of air, slugs per cubic foot
μ	Dynamic viscosity, slugs per foot second

LIST OF SYMBOLS (cont'd)

Symbol Definitions for Tabulated IBM Pressure Coefficient Data, App. II

A	Corrected angle of attack, degrees
AU	Uncorrected angle of attack, degrees
С	Airfoil chord, feet
CP	Pressure Coefficient
L	Lower surface
M	Corrected Mach Number
MU	Uncorrected Mach Number (nominal)
PO	Free stream static pressure, psf
QO	Dynamic pressure, psf
U	Upper surface

Chordwise distance from leading edge, feet

X

SUMMARY

Tests were conducted in the two-dimensional channel of the United Aircraft Corporation 8 foot wind tunnel at Mach Numbers from 0.30 to 0.80 to determine the surface pressure distributions on a Sikorsky H-34 main rotor production blade section. Twenty-nine static pressure taps were located on the upper and lower surfaces of the model. In addition three component force and moment measurements, were obtained, along with a limited amount of wake survey drag data. The pressure coefficients are tabulated for each Mach Number and angle of attack. The variation of force and moment coefficient with angle of attack at each Mach Number is also included. As the data are intended primarily for use by the National Aeronautics and Space Administration no detailed analysis has been made of the results of this test program.

INTRODUCTION

Sikorsky Aircraft, under sponsorship of the U. S. Army Transportation Research Command, USA TRECOM, (Reference I), has recently instrumented a full scale H-34 rotor blade with miniature electrical pressure transducers to permit the measurement of surface pressure distributions at various radial stations. The aircraft will be flight tested by the National Aeronautics and Space Administration to obtain instantaneous air loads on a full scale rotor in flight.

A previous wind tunnel investigation of rotor blade aerodynamic loading conducted by the NACA (References 2 and 3) showed that for a thorough evaluation of the three dimensional effects that are present on a rotor blade in flight, a knowledge of the steady-state two-dimensional pressure distributions on the same airfoil section was required as a reference. A similar basis for analysis is even more necessary for the flight test program referred to above for two reasons. First, the test is to be conducted on a production rotor blade with certain physical deviations from a true NACA 0012 profile, and consequent differences in surface pressure distributions from published data on the 0012 airfoil. Secondly, adequate pressure loading data are not available even on a true 0012 profile, in the Mach Number and angle of attack range which will be encountered in flight test.

The purpose of the present program therefore was to obtain chordwise static pressure distributions on a Sikorsky H-34 helicopter production main rotor blade section. As an addition to the primary purpose of the program, three component force and moment data, along with limited wake survey drag measurements were obtained.

This work was performed under the sponsorship of USA TRECOM, contract DA 44-177-TC-657. The results of this investigation will be used in the evaluation of the flight test data obtained from the full scale H-34 test described above.

TEST EQUIPMENT AND PROCEDURE

DESCRIPTION OF TEST FACILITY

The United Aircraft Corporation two-dimensional channel is composed of a special insert in the U.A.C. large subsonic wind tunnel. This wind tunnel is powered by a 9,000 horsepower motor and has interchangeable octagonal test sections of 8 feet and 18 feet across the flats. The twodimensional airfoil test channel consists of two identical sidewalls which are inserted in the 8-foot octagonal test section to form a rectangular test region and two trapezoidal outer passages (see Figure 1). The channel, 125 inches long provides a test section 93 inches high and 33 inches wide. Airfoils are mounted with their pitching axis 66 inches downstream of the channel leading edge to insure minimum effect of model attitude on test section velocity. Linkages and support struts connected to the electromechanical balance beneath the tunnel extend up through the hollow sidewalls and are attached to the model spar by end fittings. The mechanical balance measures lift and drag forces directly. A Baldwin-Lima-Hamilton bending beam equipped with strain gages is used to obtain pitching moment. A wake survey rake had been installed for a previous test and was used to afford an alternate means of obtaining drag measurements. It consisted of 46 total pressure tubes and 2 static pressure tubes located 39 inches downstream of the model supports.

DESCRIPTION OF MODEL

The model was made from an untwisted portion of a production Sikorsky H-34 main rotor blade, consisting of an extruded spar and three trailing edge pockets. The outer two trailing edge pockets were formed of bonded "honeycomb" covered with a sheet aluminum skin. The center pocket construction consisted of one stainless steel rib in the center of the pocket and four aluminum ribs, evenly spaced and covered with sheet aluminum skin. This center pocket construction provided the space necessary for the installation of the twenty-nine surface static pressure taps consisting of .0625 inch diameter stainless steel tubing, which in turn were plumbed to a manometer board. The pressure orifices were located at half span at the following stations (upper and lower surfaces), expressed in percent of chord: 0, 0.8, 1.7, 4.0, 6.5, 9.0, 13.0, 16.8, 23.3, 33.5, 50.0, 62.5, 76.9, 91.5, and 96.0. The trailing edge pocket was then filled with plastic foam to stiffen the skin and prevent any possibility of panel flutter at severe loading conditions. The model has a total chord of 16.4 inches and a span of 32.70 inches, with an NACA 0012 profile based on a chord of 16.0 inches, modified by a 0.4 inch trailing edge tal extension .096 inches thick. (This trailing edge tab may be deflected upward to approximately a three degree angle during production testing of the full scale blade to assure proper track and balance). A view of the instrumented blade section is shown in figure 2, and a comparison of the contour at half-span of the test airfoil with the contour of a true NACA 0012 section is presented in figure 3.

TEST PROCEDURE

The model was tested at nominal Mach Numbers of 0.30, 0.40, 0.50, 0.60, 0.65, 0.70, 0.75, and 0.80, at angles of attack ranging from -4 degrees to 26 degrees at the lowest Mach Numbers. The maximum angles of attack at the higher Mach Numbers were limited by the tunnel power available. The Reynolds Numbers corresponding to the test conditions are shown in figure 4.

The model was also tested with the trailing edge tab deflected upwards at the standard production test angle at Mach Numbers of 0.30, 0.40, 0.50, 0.60, 0.70, and 0.80. This was done to obtain data to aid in the evaluation of results from the full scale rotor blade test, for which the trailing edge tab was deflected for a short spanwise distance near the tip to provide proper track and balance.

The static pressures on the model were recorded by photographing a mercury manometer board. The values of force balance—lift, drag, and pitching moment were manually recorded. A wake survey rake had been installed in the test section for use in the preceding test program, and the pressures obtained during the early portion of the present test were recorded to afford a check on the drag obtained with the balance. However, the wake rake supports failed after a Mach Number of .6 was obtained and no further data could be acquired.

DATA REDUCTION AND REPEATABILITY

REDUCTION OF DATA

The magnitude of the manometer tube pressures were recorded on IBM cards by means of a manually operated electro-mechanical film reader. An IBM 704 electronic data processing machine program was then used to compute the corrected pressure coefficient, corrected Mach Number, and corrected angle of attack.

The force balance data were immediately reduced to corrected coefficient form by the use of a small electronic computer. The force coefficient data were continuously plotted to produce a current record of the results during the program.

The wake drag data were reduced using the tables and charts of Reference 4. This method assumes that the wake drag coefficient is proportional to the total head loss in the airfoil wake, and further assumes that the variation of total head loss across the wake has the typical form (resembling a cycle of a cosine squared curve).

Tunnel wall corrections were applied to all the foregoing data using the equations of Reference 5.

REPEATABILITY OF DATA

Previous tunnel balance calibrations have shown the balance to be repeatable to ± 1.25 pounds of lift, ± 0.3 pounds of drag, and ± 1.5 foot pounds of pitching moment for steady loads. The average zero shift for all runs was ± 0.8 pounds of lift, ± 0.5 pounds of drag, and ± 0.5 foot pounds of pitching moment.

The estimated average variations in aerodynamic parameters with Mach Number as determined from analysis of the present data, are shown in the following tabulation:

Nominal Mach Number	<u>0. 4</u>	<u>0.6</u>	0.8	
M	±.003	± 002	±. 002	
a	± 20 min.	± 20 min.	± 20 min.	
Cp	± 026	±.014	±.009	
C _p CL	±.010	±. 006	±.004	
$C_{\mathbf{D}}$	±.0013	±.0010	±.0010	
Cm	±.003	±.001	±.001	

Although all of the data obtained during the test have been presented for the sake of completeness, care should be taken in interpreting the data at high angles of attack, due to possible interference caused by the tunnel walls. Discrepancies between the force balance and wake survey drag coefficients are discussed in the section entitled "Presentation of Results."

PRESENTATION OF RESULTS

A portion of the pressure data has been plotted in the form of surface pressure coefficient versus chordwise distance from the airfoil leading edge at four angles of attack for each of eight Mach Numbers. Figures 5 through 20 present these data obtained with zero tab deflection and figures 21 through 32 present similar data for the production tab deflection.

The force and moment data are presented in figures 33 through 46 in the form of lift, drag, and pitching moment coefficient versus angle of attack. Figures 33 through 40 present data obtained at the various Mach Numbers with no trailing edge tab deflection. To afford a correlation between the measured lift coefficients and the pressure coefficients a certain amount of the plotted pressure distributions were integrated to yield the normal force coefficient. Multiplying this normal force coefficient by the cosine of the airfoil angle of attack yields an approximate CL which was then spotted on the curves obtained with the force balance. The agreement is generally quite reasonable although the approximate lift coefficients determined from the integrated pressures are frequently less than the balance data.

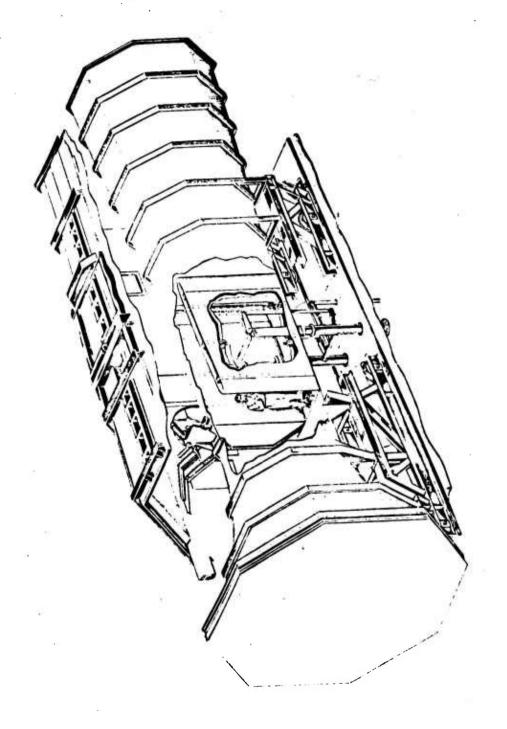
Figures 33 to 36 also compare the drag coefficients as determined from the force balance and those measured by the wake survey rake for those conditions where both measurements were obtained. As discussed in Reference 6, it is inherently difficult to obtain two-dimensional drag data from a force balance, which measures the average drag on the model, where three dimensional effects such as the end gap and the sidewall boundary layer are present. Therefore, the wake survey data are more representative of the true two-dimensional drag forces at low angles of attack. At high angles of attack or in the presence of shocks however, the procedure used to compute the drag can lead to excessive errors. Inasmuch as the wake survey data were limited to but a few conditions, both sources of data are presented for the sake of completeness. Above a Mach Number of .65 the force balance data agree favorably with previous Sikorsky tests of production airfoil sections.

Figures 4l through 46 present data obtained with the trailing edge tab of the model deflected upward at the standard production test angle, approximately three degrees. Results for those data points which exceed the figure limits are presented in Appendix I. Although no wake survey drag data are available for the deflected tab condition, differences between the balance and the wake survey drags similar to the undeflected tab condition would be expected.

All of the pressure data obtained during the investigation are presented in tabular form in Appendix II in the form of pressure coefficients at each chordwise location. Also listed are the Mach Numbers and angles of attack, both corrected and uncorrected, the dynamic pressure, and the free stream static pressure corrected for tunnel wall effects. The run number is also listed to facilitate correlation of pressure distributions with force balance measurements.

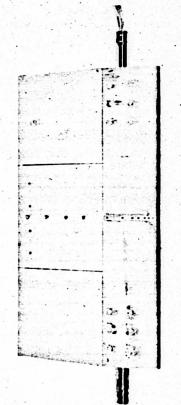
REFERENCES

- 1. Installation of Instrumentation for Dynamic Airloads on Helicopter Rotor Blades, USA TRECOM Contract DA 44-177-TC-547.
- 2. Rabbott, John P., Jr., Static Thrust Measurements of the Aerodynamic Loading on a Helicopter Rotor Blade, NACA TN 3688, July, 1956.
- 3. Rabbott, John P., Jr., and Churchill, Cary B., Experimental Investigation of the Aerodynamic Loading on a Helicopter Rotor Blade in Forward Flight, NACA RM L56107, October, 1956.
- 4. Block, M. J., and Katzoff, S.,. Tables and Charts for the Evaluation of Profile Drag from Wake Surveys at High Subsonic Speeds, NACA RB No. L5Fl5a, July, 1945.
- 5. Allen, J. J. and Vincenti, W. G., Wall Interference in a Two-Dimensional Flow Tunnel, with Consideration of the Effects of Compressibility, NACA Report 782, 1944.
- 6. Loftin, Laurence K. and Smith, Hamilton A., Aerodynamic Characteristics of 15 NACA Airfoil Sections at Seven Reynolds Numbers from 0.7 x 10⁶ to 9.0 x 10⁶, NACA TN 1945, October, 1956.





H-34 MAIN ROTOR SECTION



TOP SURFACE

BOTTOM SURFACE

FIGURE 2. H-34 WIND TUNNEL MODEL

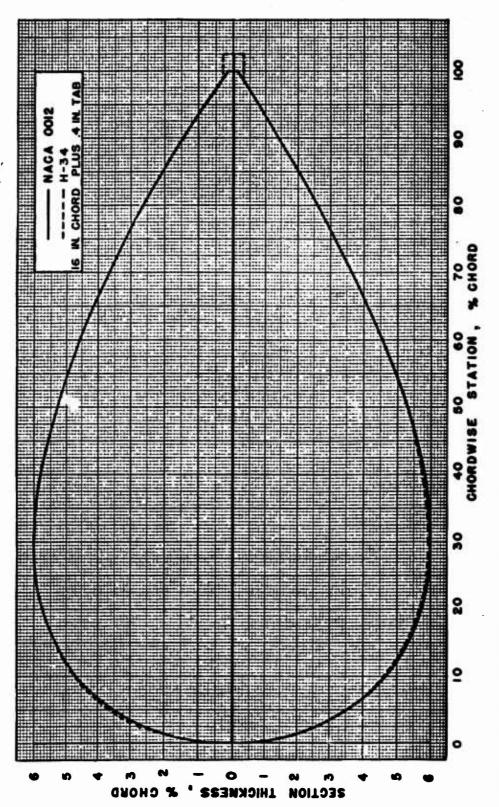


FIGURE 3. AIRFOIL CONTOUR IN COMPARISON TO NACA DOIZ SECTION

H-34 AIRFOIL AT 1/2 SPAN

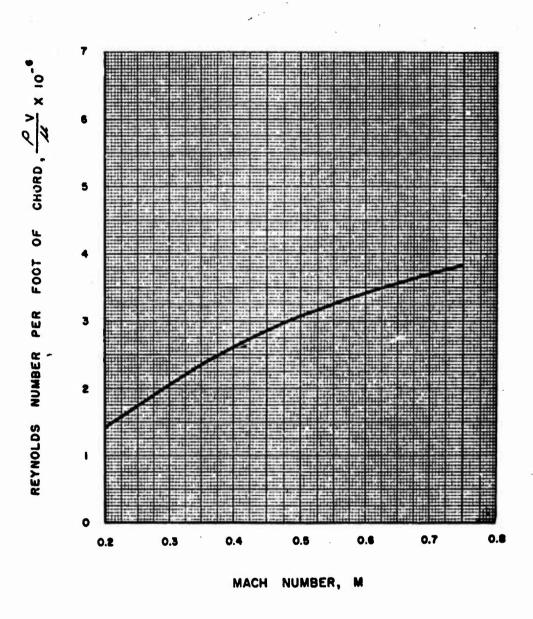


FIGURE 4. VARIATION OF REYNOLDS NUMBER WITH MACH NUMBER

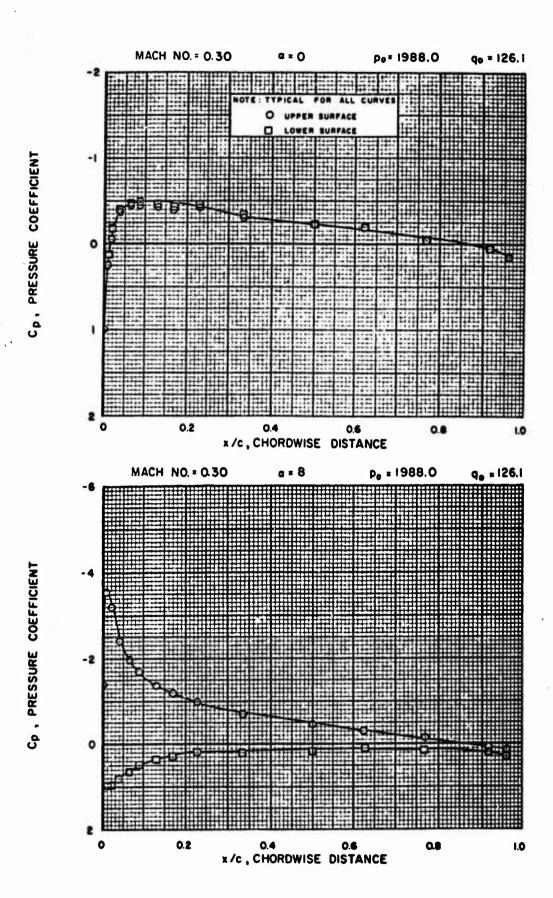


FIGURE 5 CHORDWISE PRESSURE COEFFICIENTS

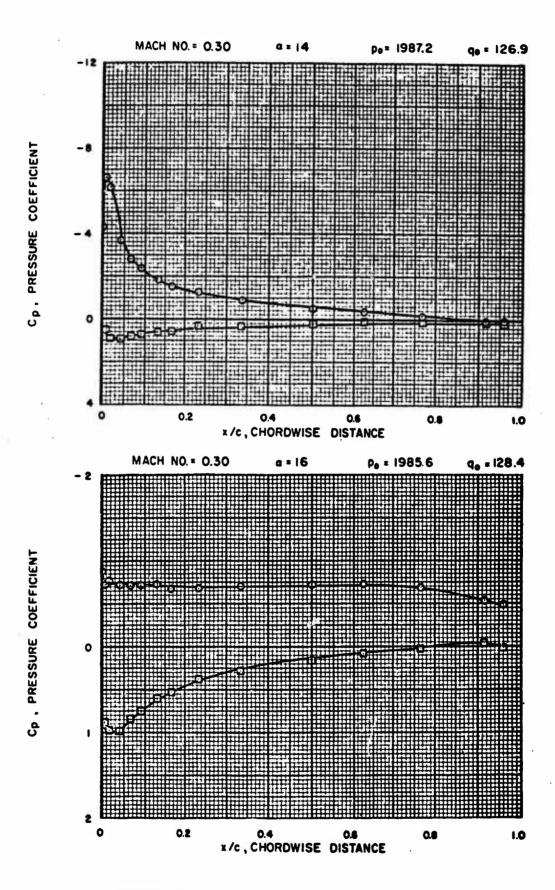


FIGURE 6 CHORDWISE PRESSURE COEFFICIENTS

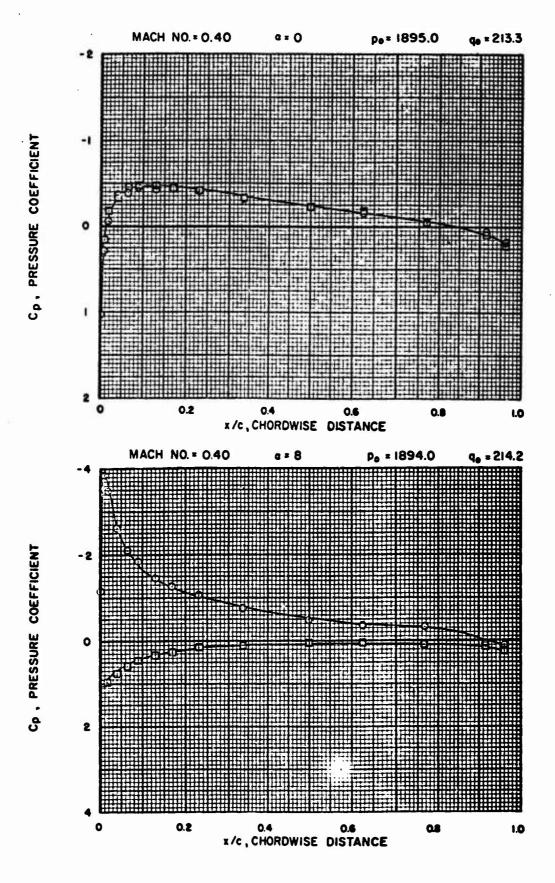


FIGURE 7 CHORDWISE PRESSURE COEFFICIENTS

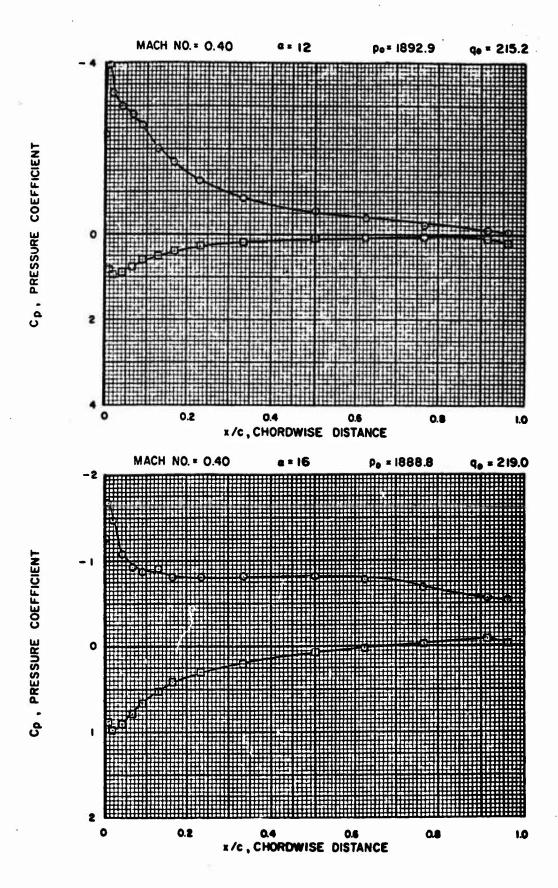


FIGURE 8 CHORDWISE PRESSURE COEFFICIENTS

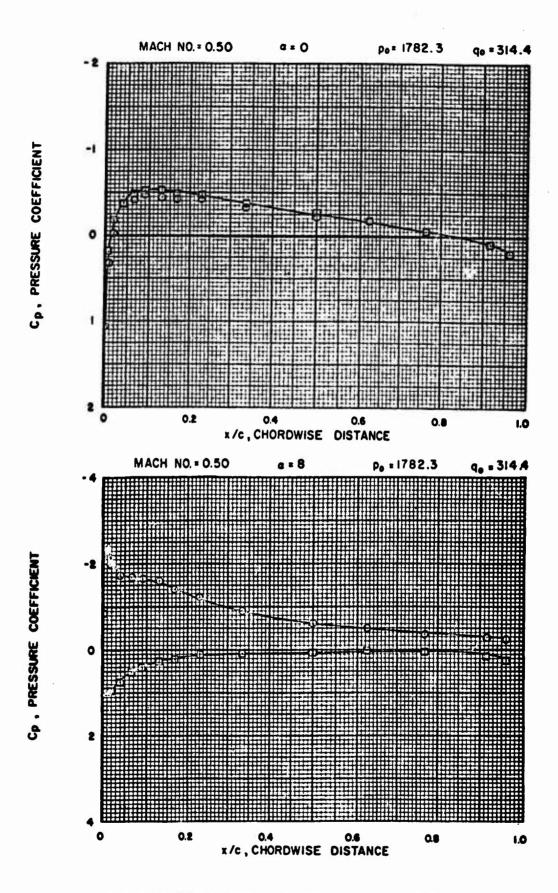


FIGURE 9 CHORDWISE PRESSURE COEFFICIENTS

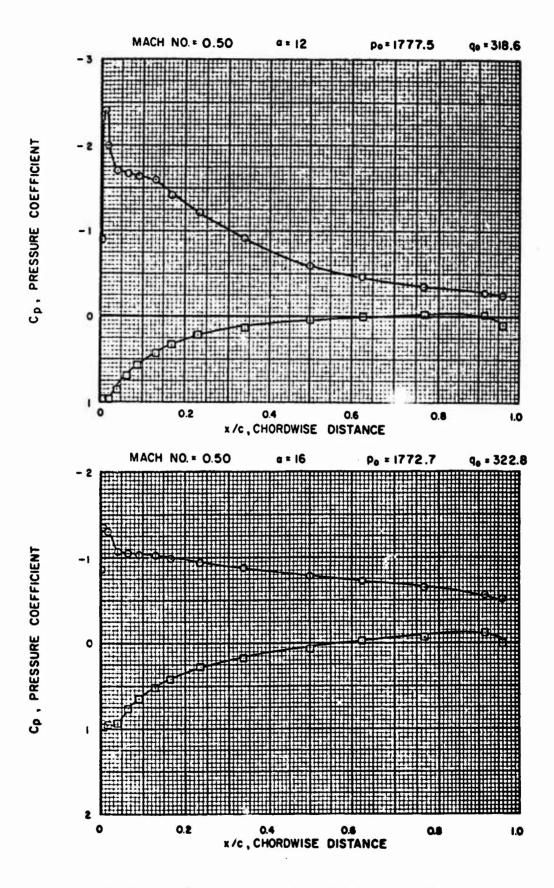


FIGURE 10 CHORDWISE PRESSURE COEFFICIENTS

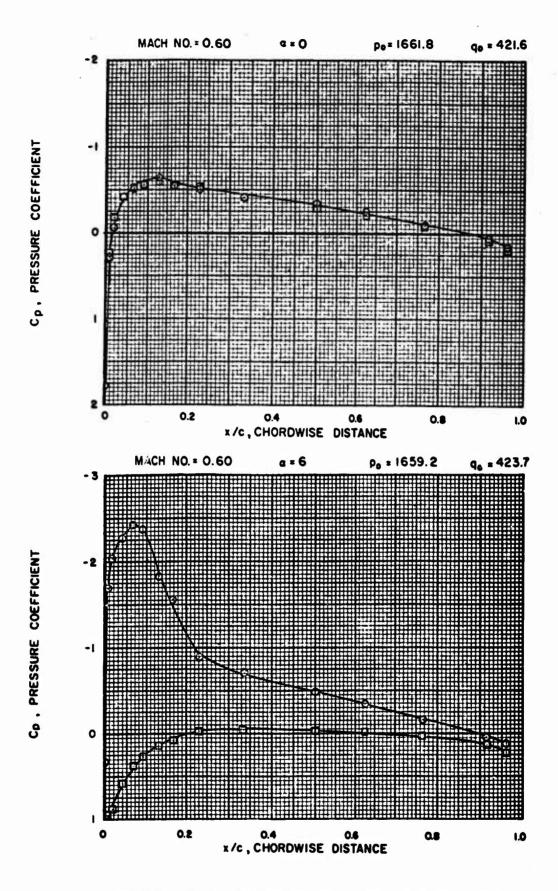


FIGURE II CHORDWISE PRESSURE COEFFICIENTS

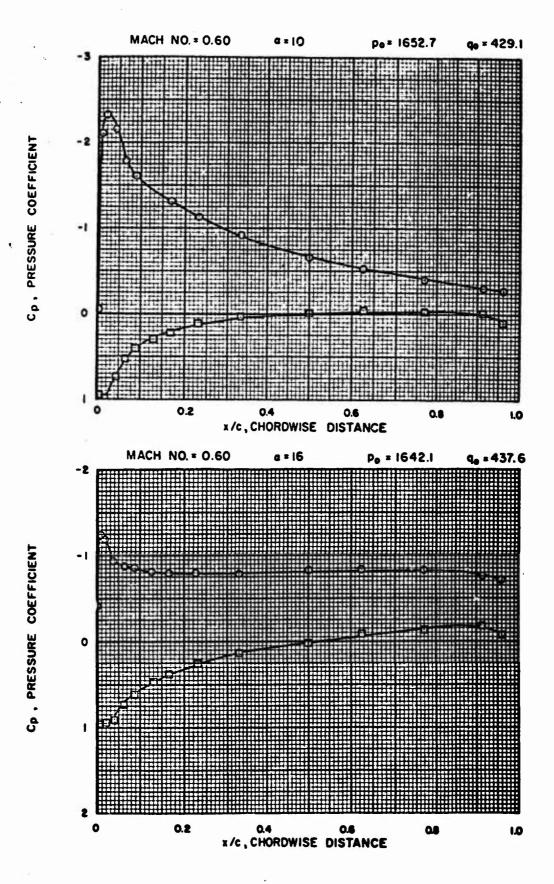


FIGURE 12 CHORDWISE PRESSURE COEFFICIENTS

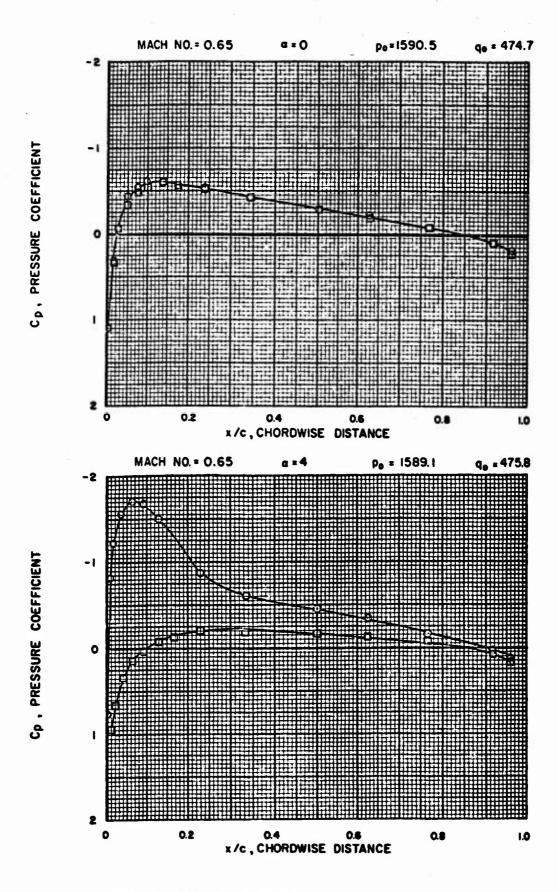


FIGURE 13 CHORDWISE PRESSURE COEFFICIENTS

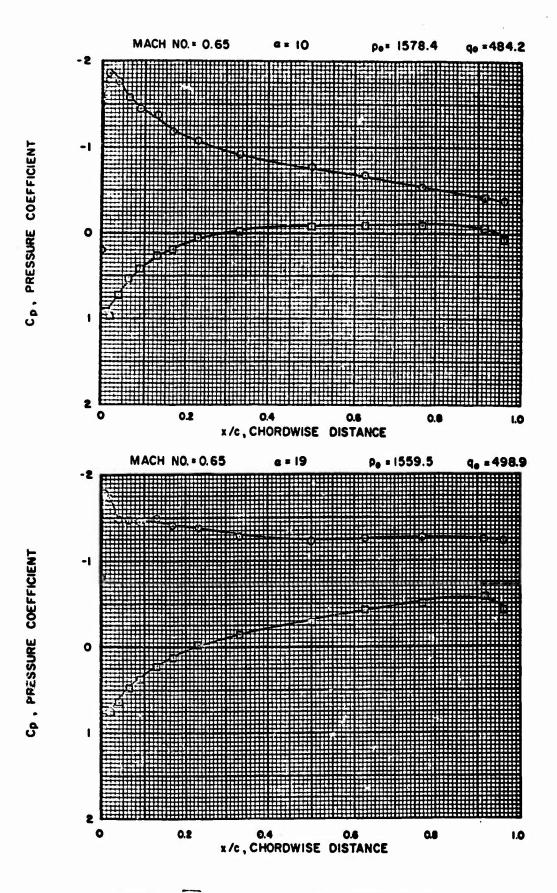


FIGURE 14 CHORDWISE PRESSURE COEFFICIENTS

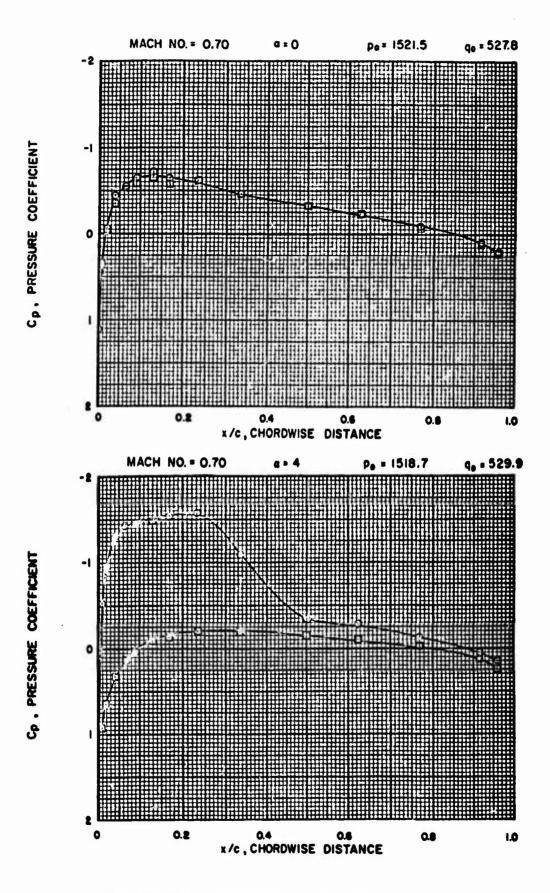


FIGURE 15 CHORDWISE PRESSURE COEFFICIENTS

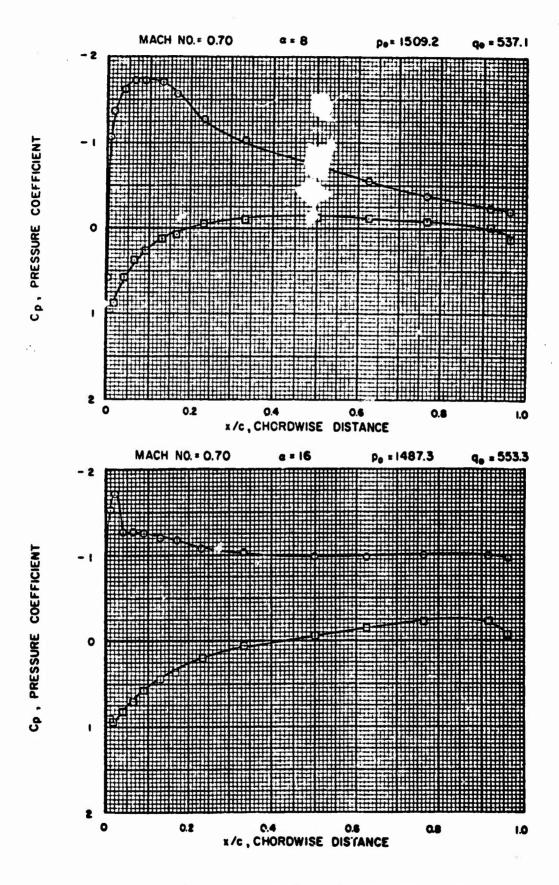


FIGURE 16 CHORDWISE PRESSURE COEFFICIENTS

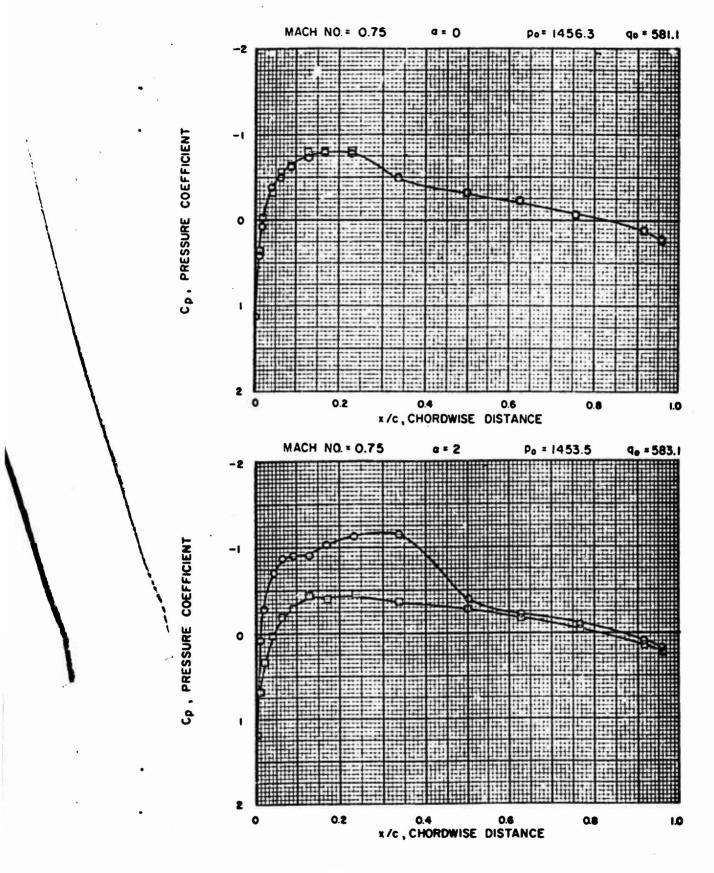


FIGURE 17 CHORDWISE PRESSURE COEFFICIENTS

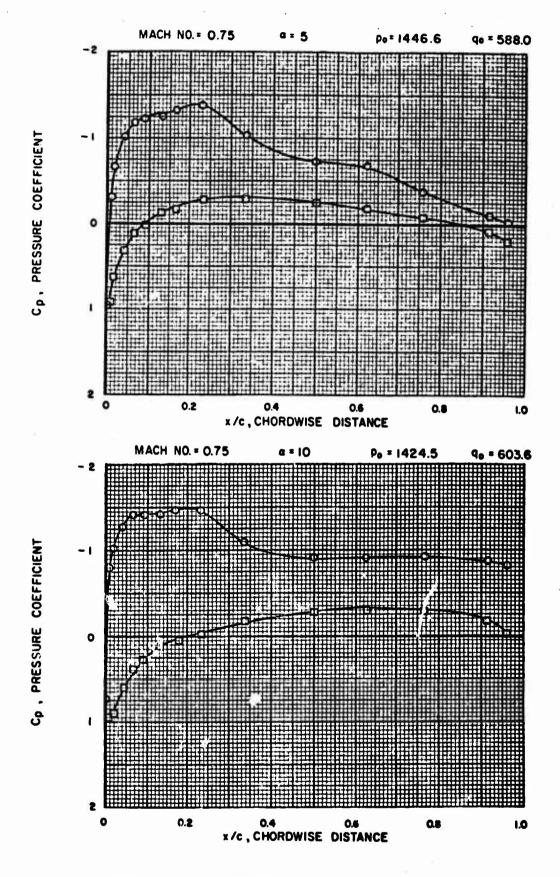


FIGURE 18 CHORDWISE PRESSURE COEFFICIENTS

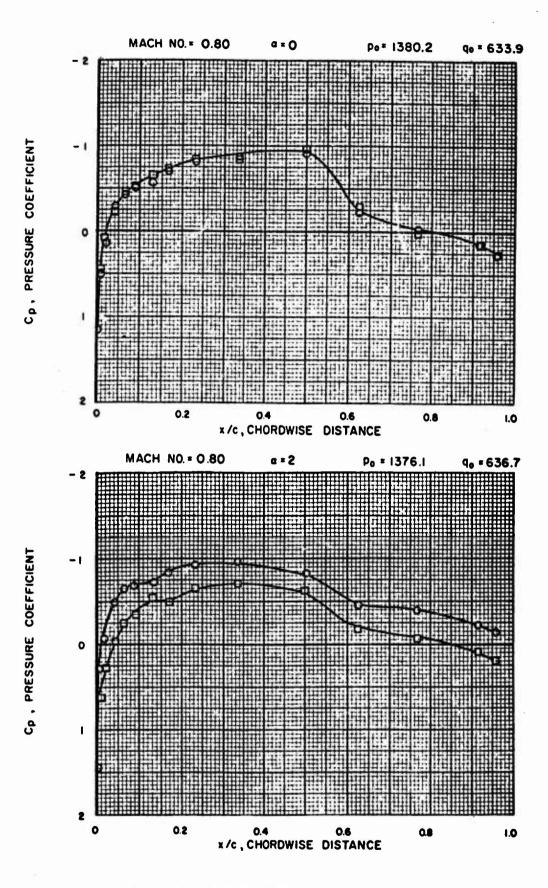


FIGURE 19 CHORDWISE PRESSURE COEFFICIENTS

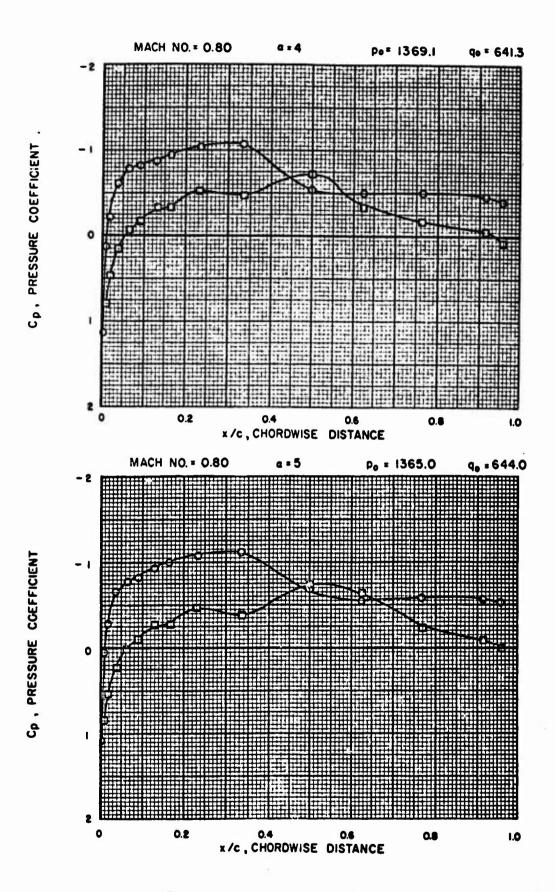


FIGURE 20 CHORDWISE PRESSURE COEFFICIENTS

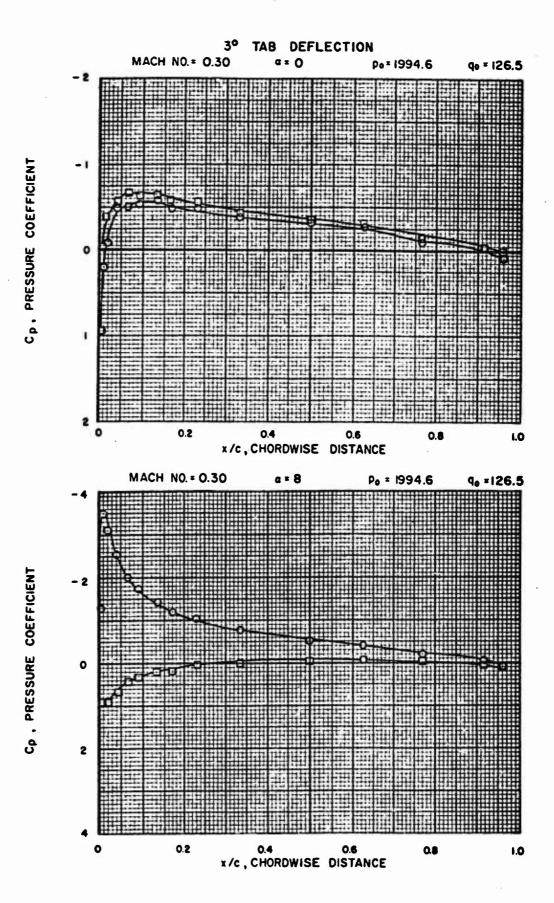


FIGURE 21 CHORDWISE PRESSURE COEFFICIENTS

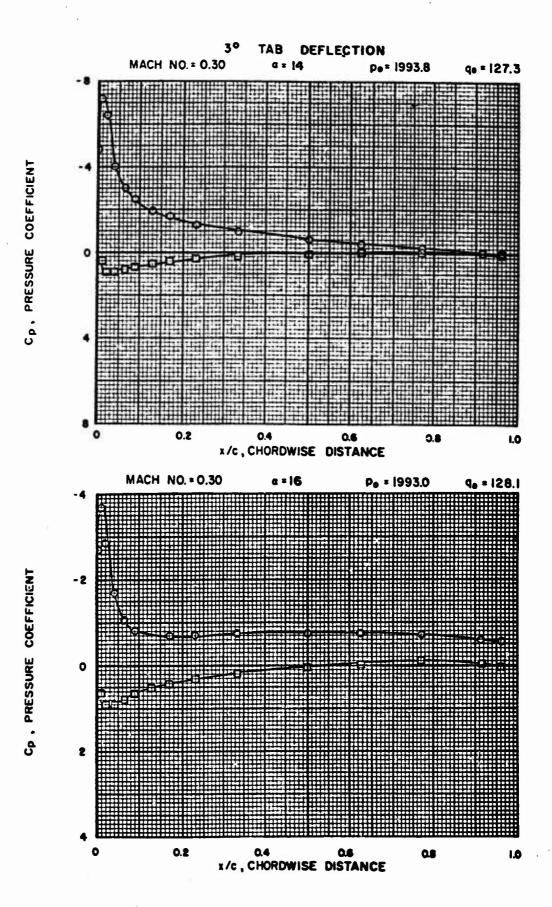


FIGURE 22 CHORDWISE PRESSURE COEFFICIENTS

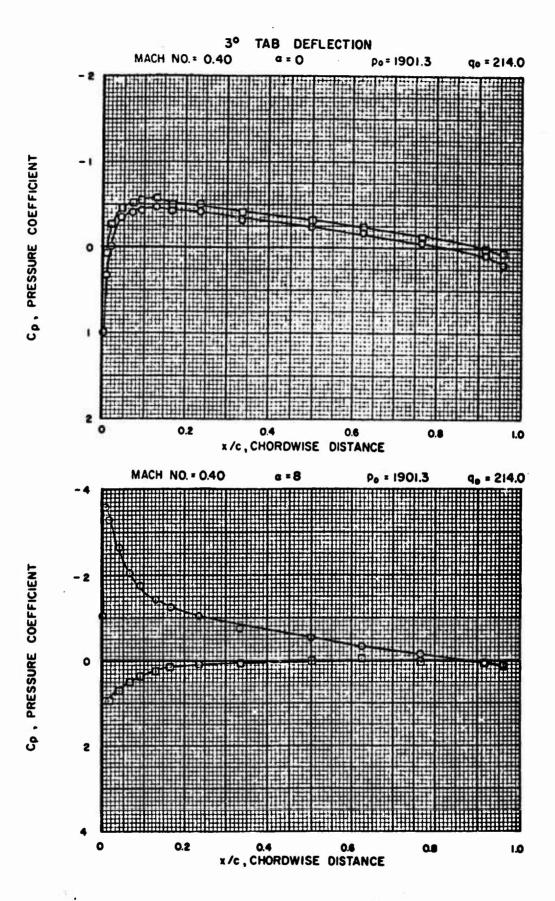


FIGURE 23 CHORDWISE PRESSURE COEFFICIENTS

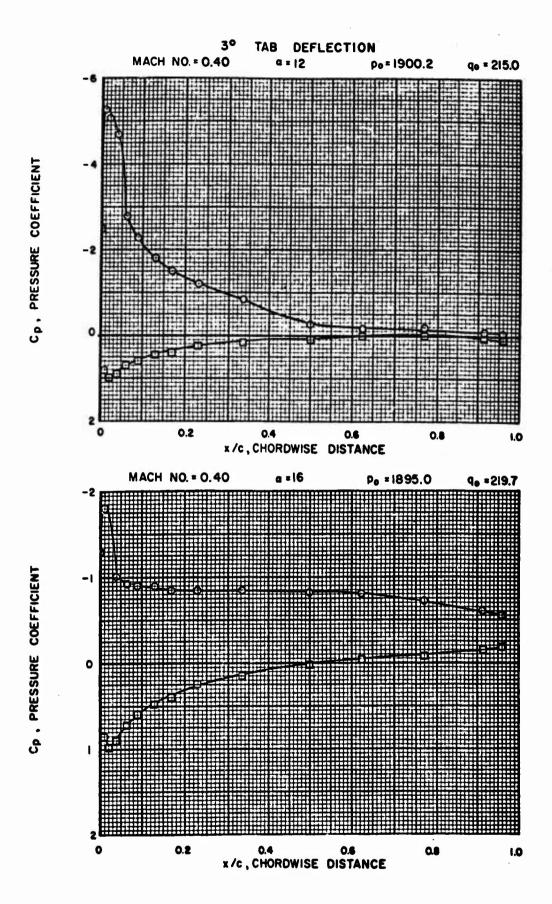


FIGURE 24 CHORDWISE PRESSURE COEFFICIENTS

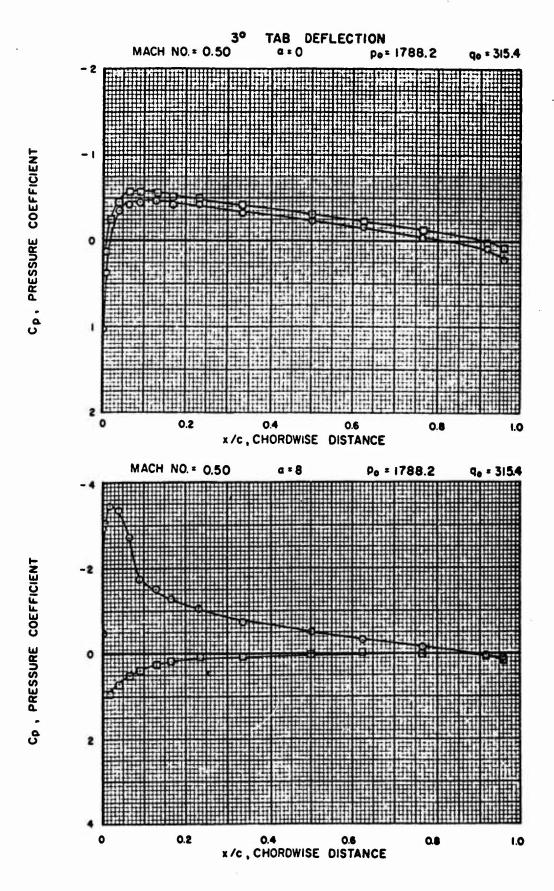


FIGURE 25 CHORDWISE PRESSURE COEFFICIENTS

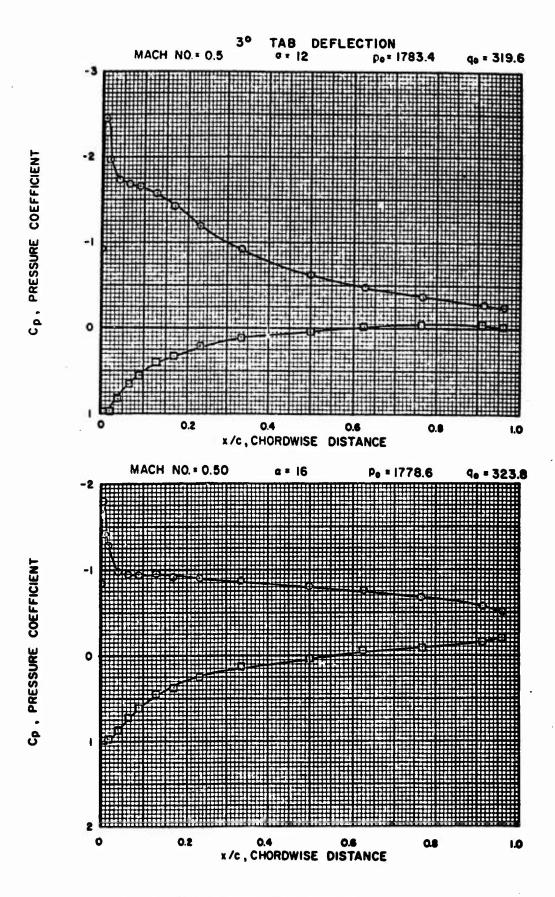


FIGURE 26 CHORDWISE PRESSURE COEFFICIENTS

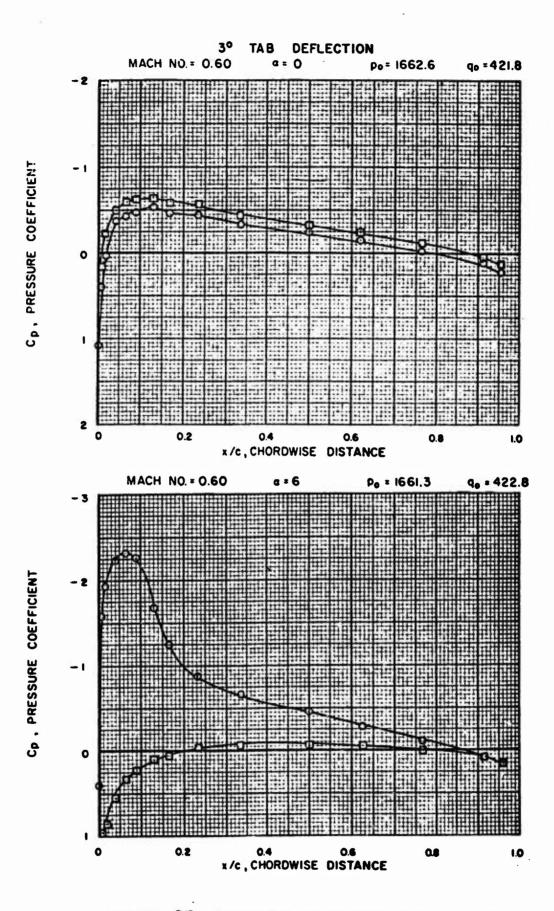


FIGURE 27 CHORDWISE PRESSURE COEFFICIENTS
35

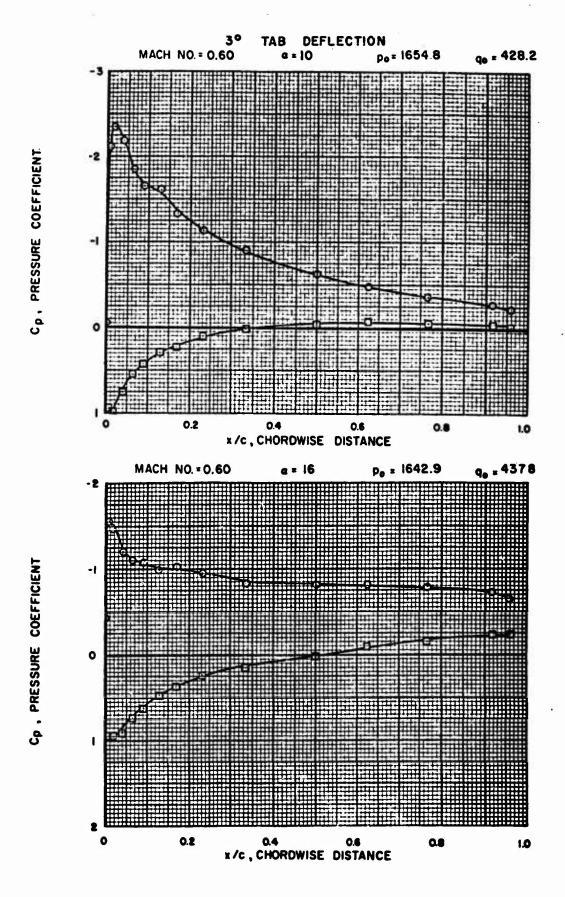


FIGURE 28 CHORDWISE PRESSURE COEFFICIENTS

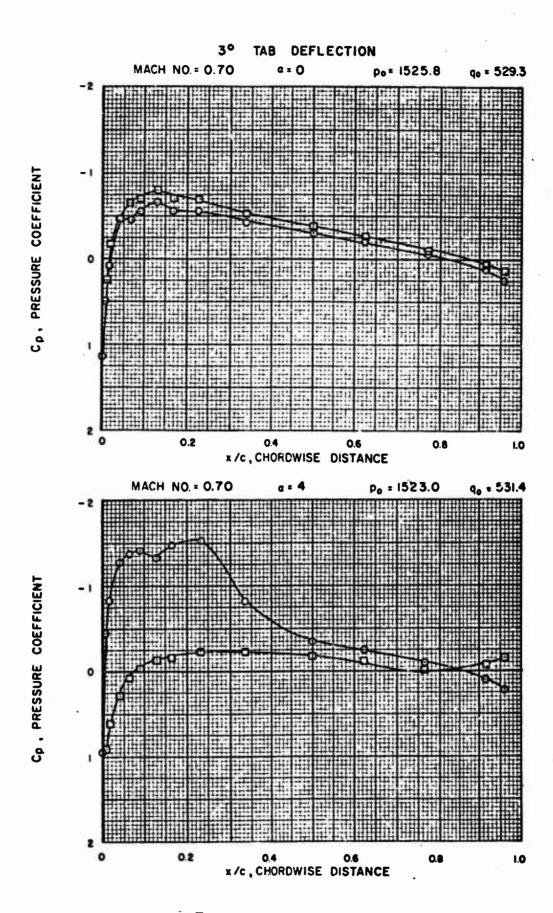


FIGURE 29 CHORDWISE PRESSURE COEFFICIENTS

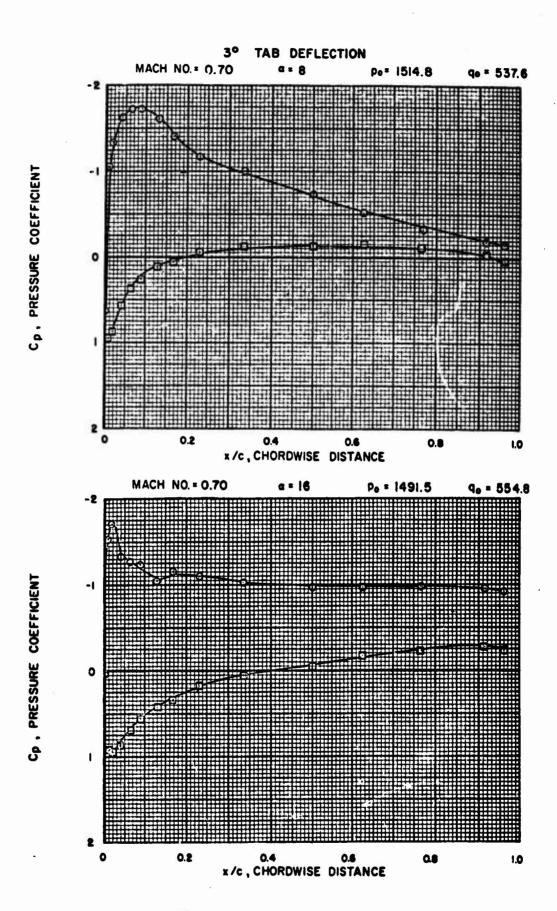


FIGURE 30 CHORDWISE PRESSURE COEFFICIENTS

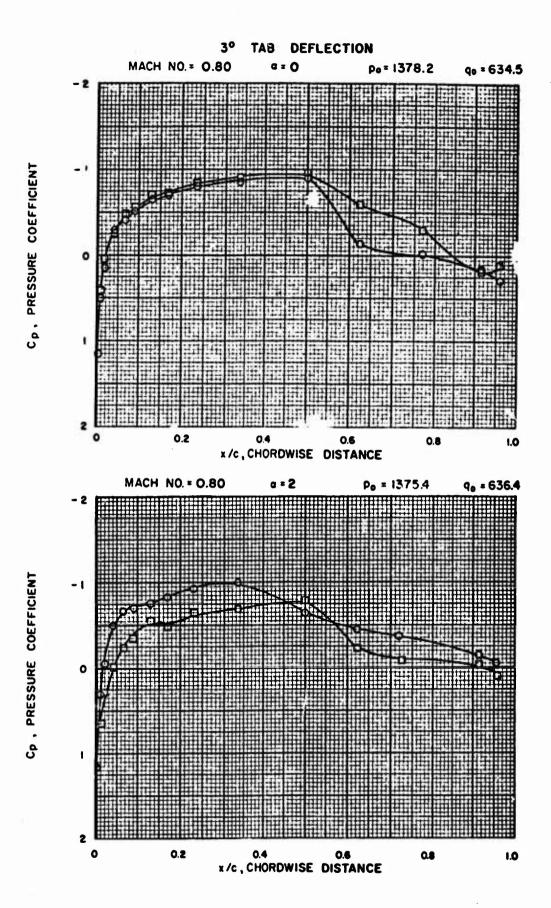


FIGURE 31 CHORDWISE PRESSURE COEFFICIENTS

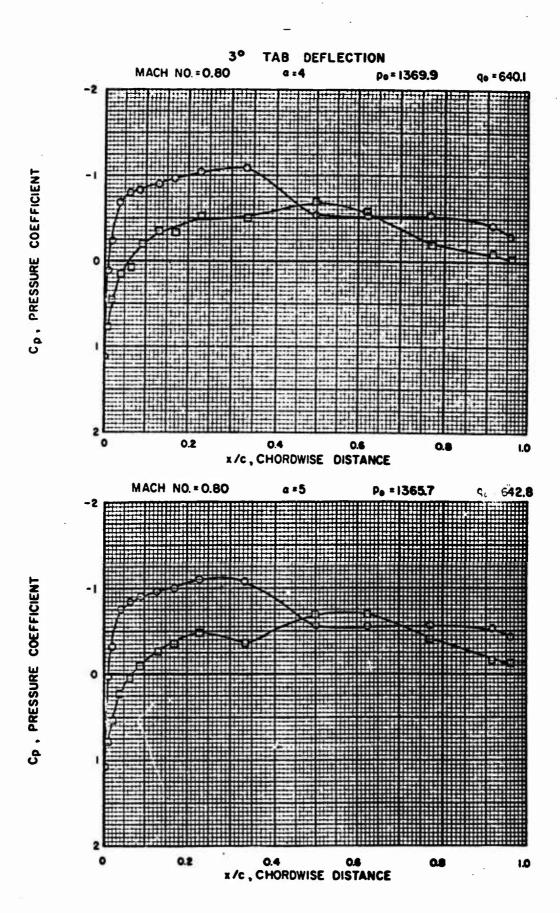


FIGURE 32 CHORDWISE PRESSURE COEFFICIENTS

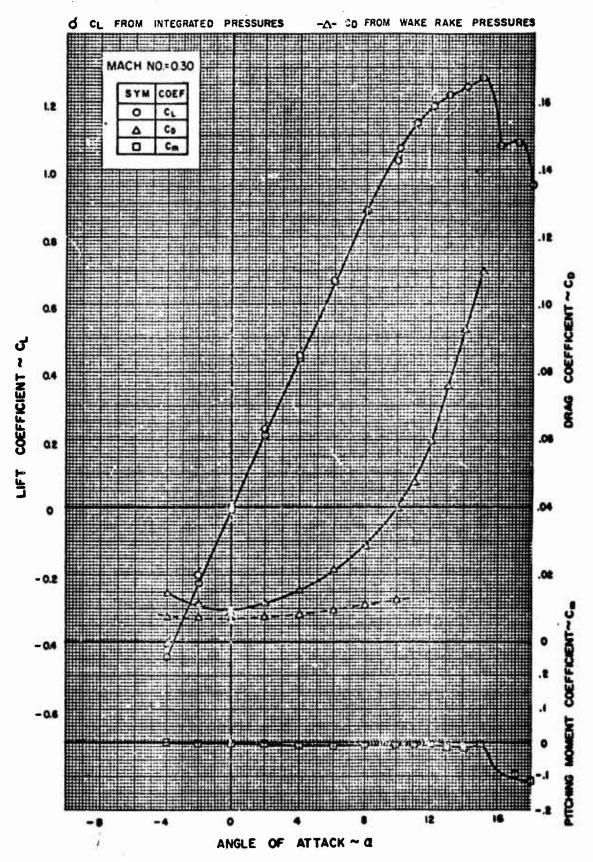


FIGURE 33. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

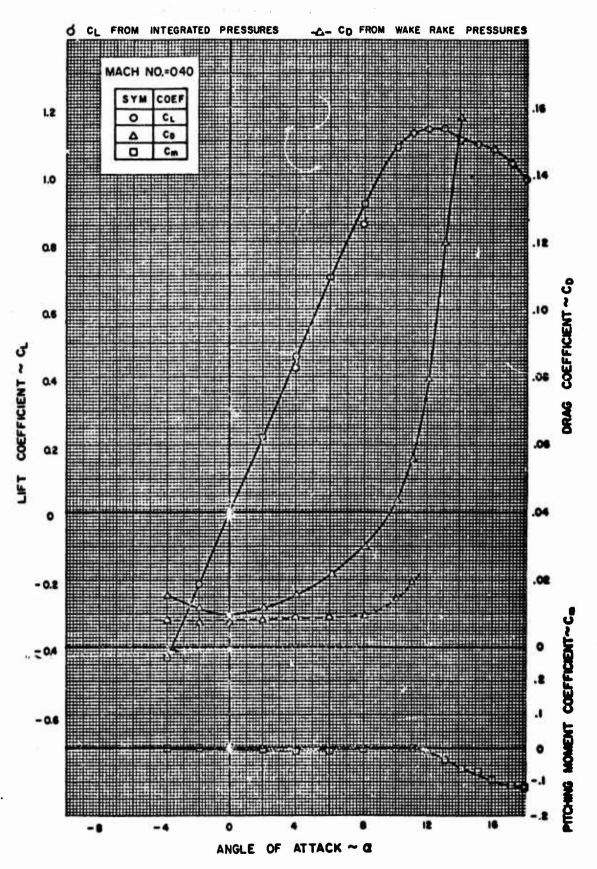


FIGURE 34. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

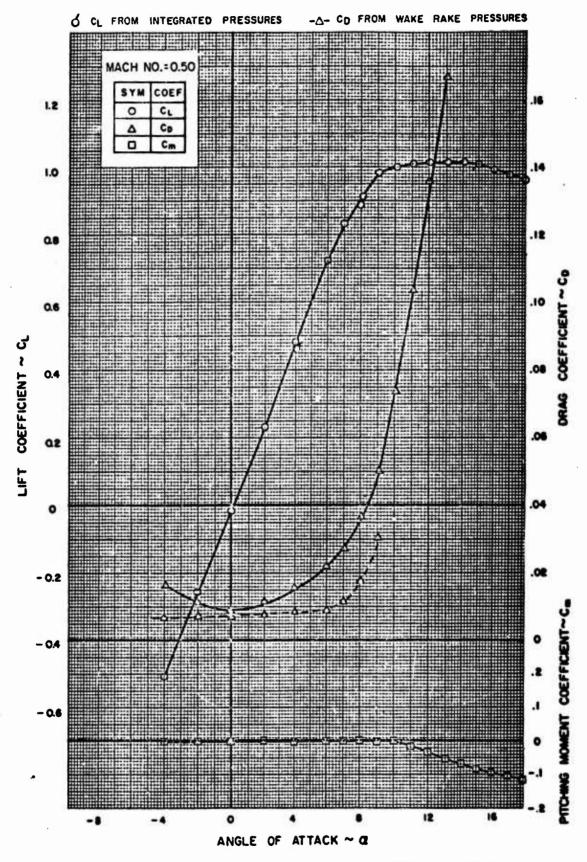


FIGURE 35. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

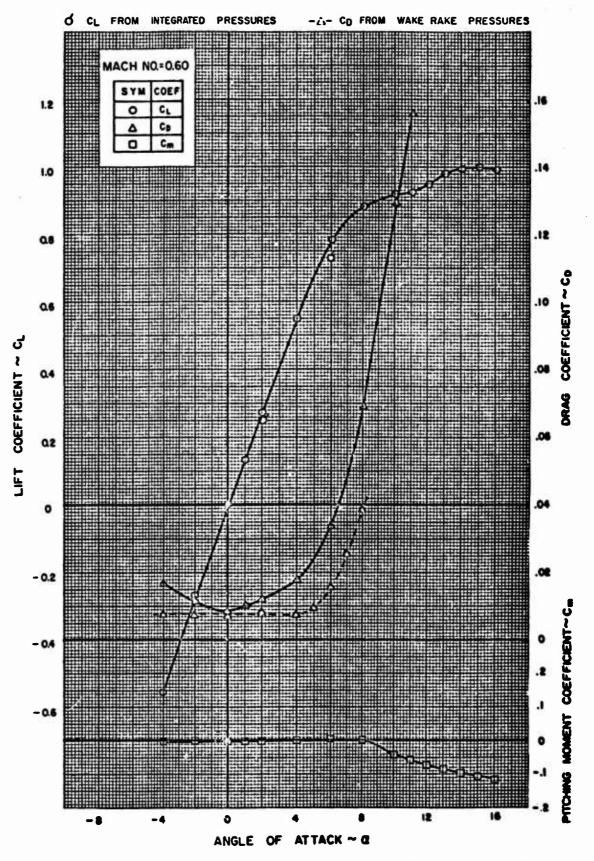


FIGURE 36. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

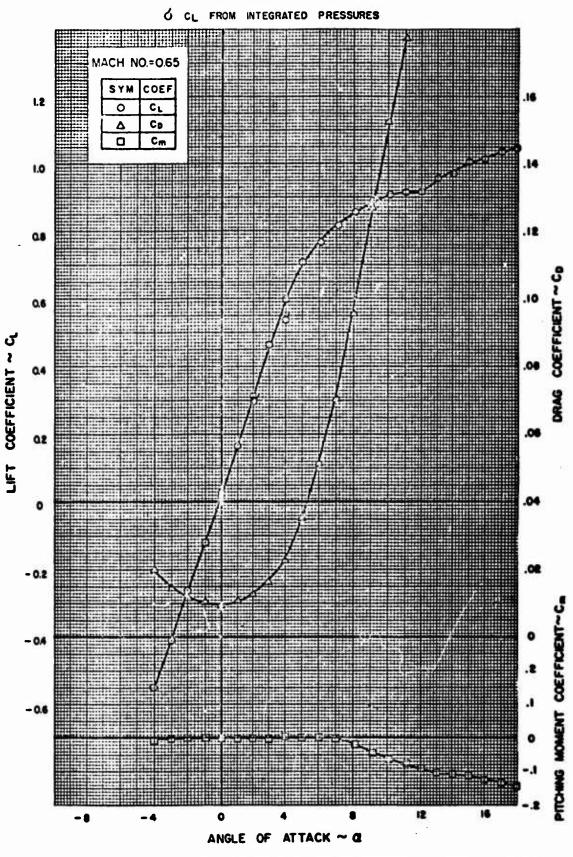


FIGURE 37. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

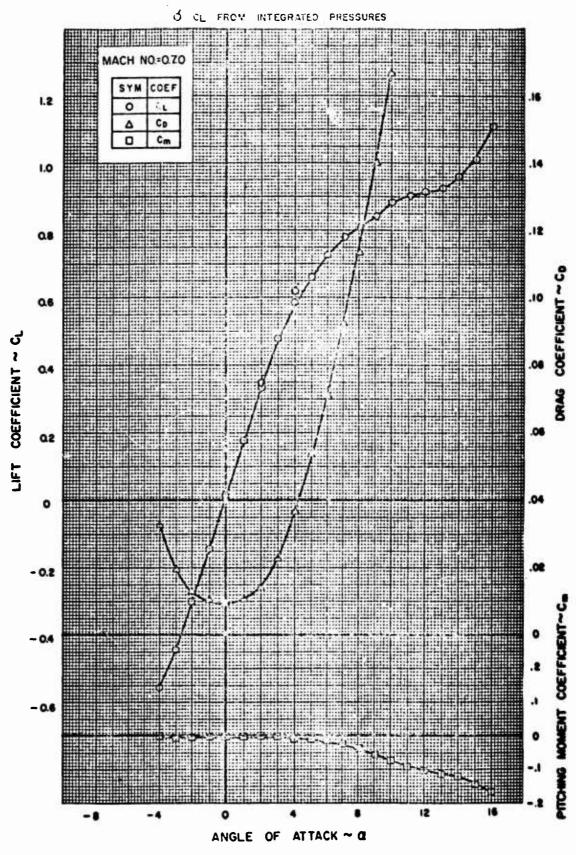


FIGURE 38. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

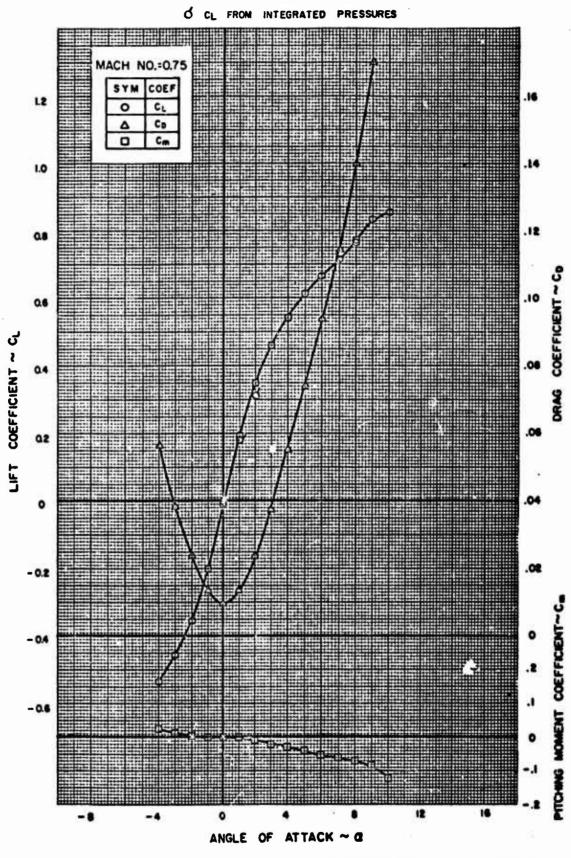


FIGURE 39. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

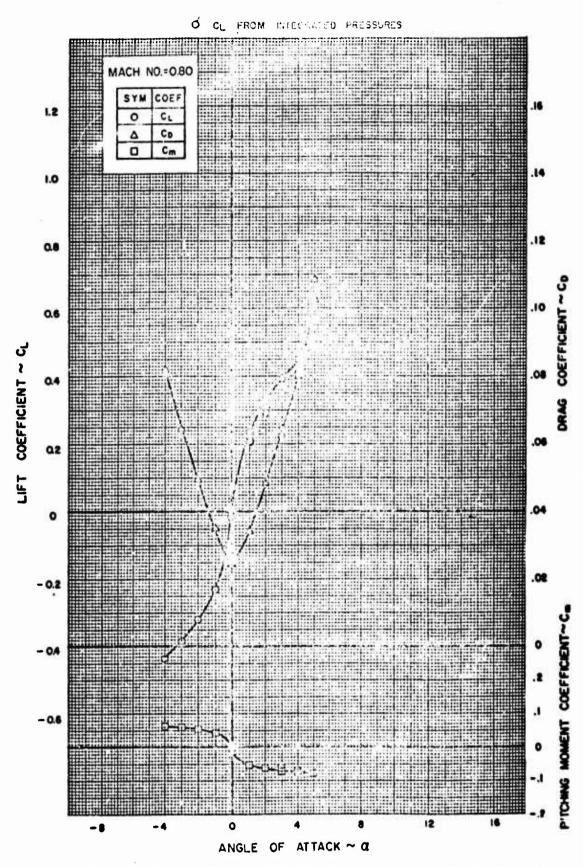


FIGURE 4Q VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

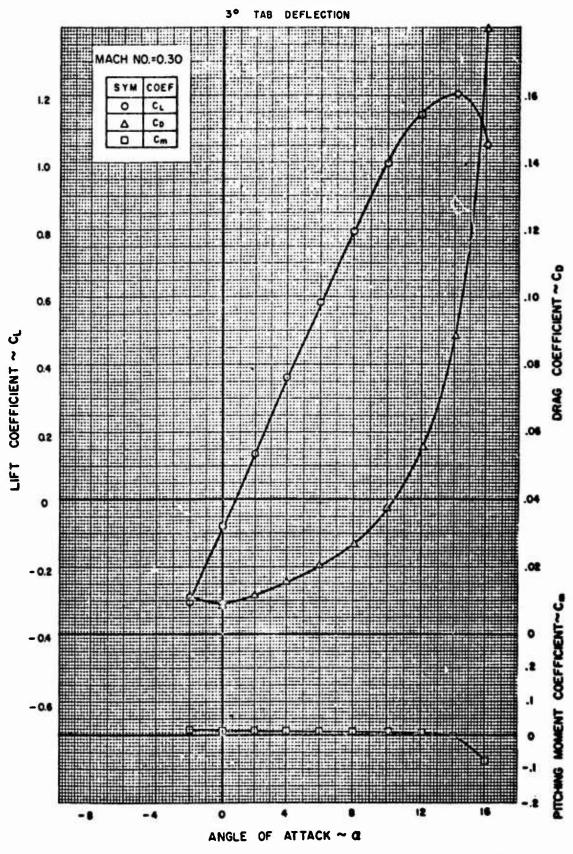


FIGURE 41. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

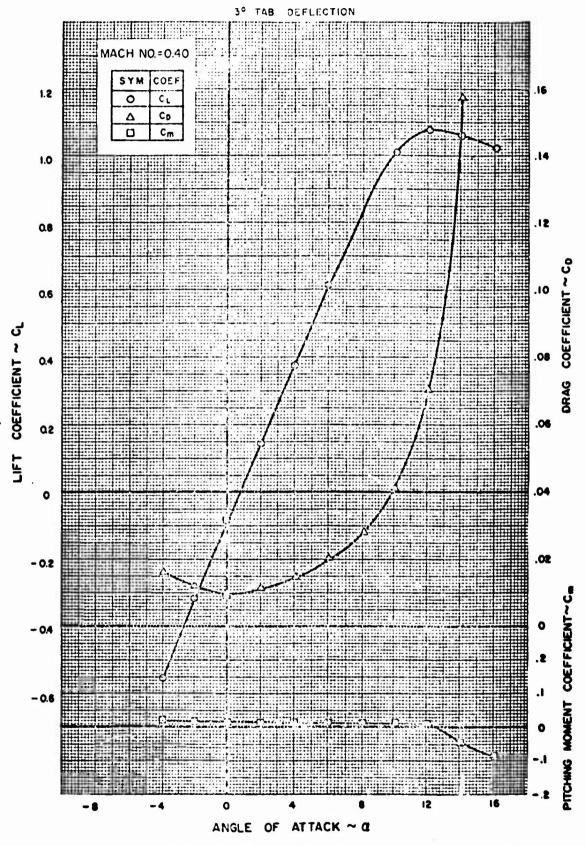


FIGURE 42. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

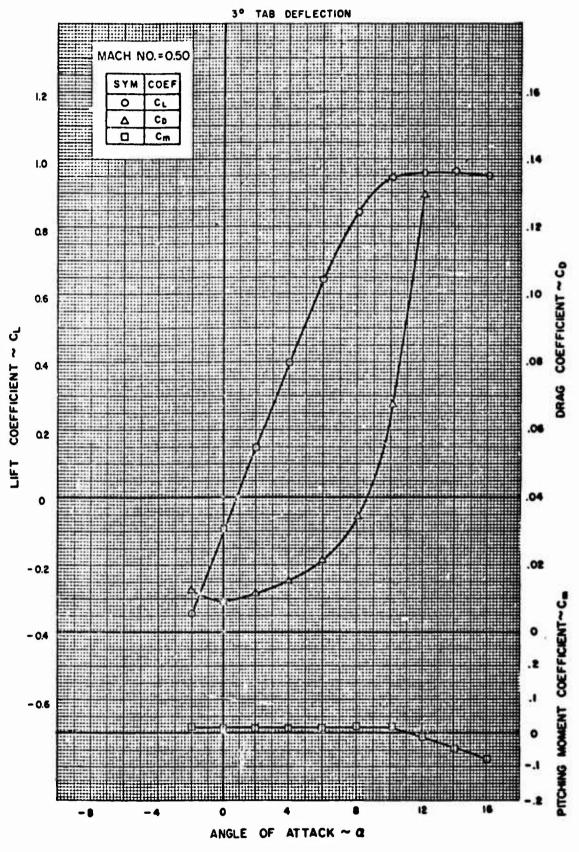


FIGURE 43. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

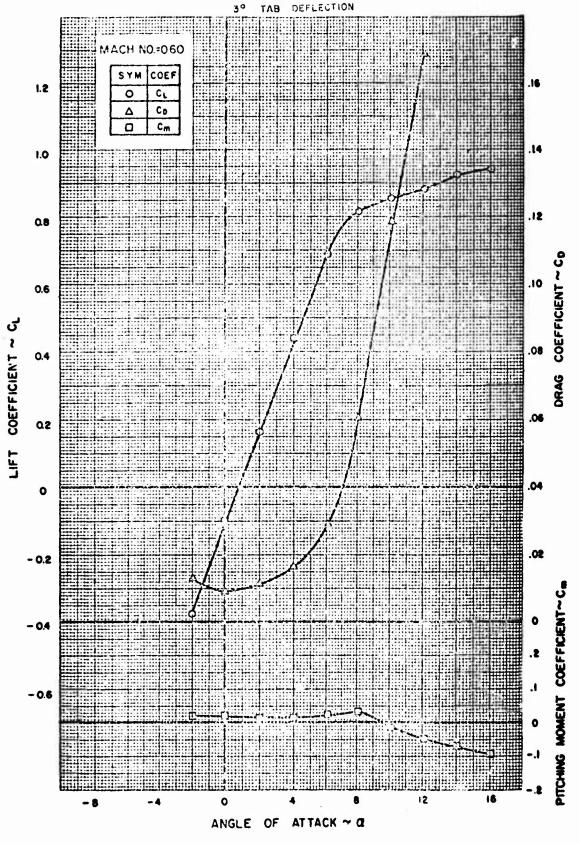
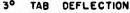


FIGURE 44. VARIATION OF FORCE COEFFICIENTS WITH ANGLE
OF ATTACK



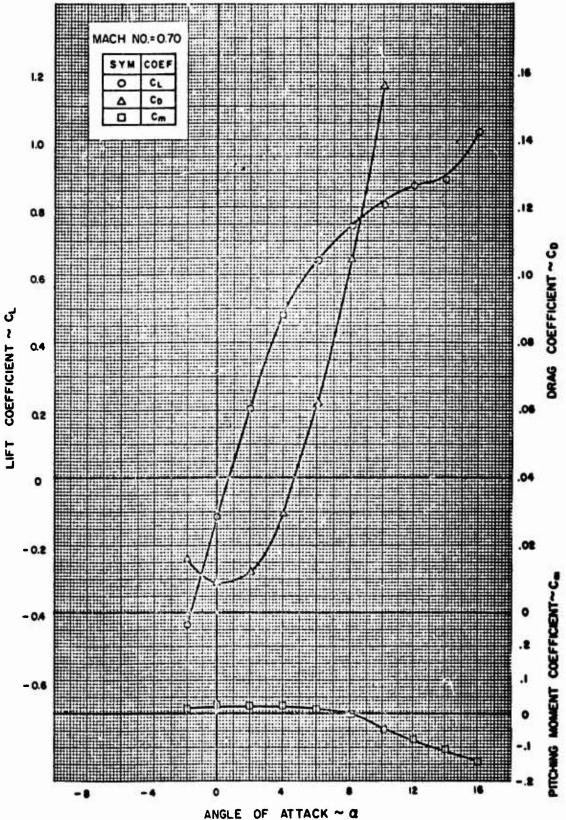


FIGURE 45. VARIATION OF FORCE COEFFICIENTS WITH ANGLE
OF ATTACK

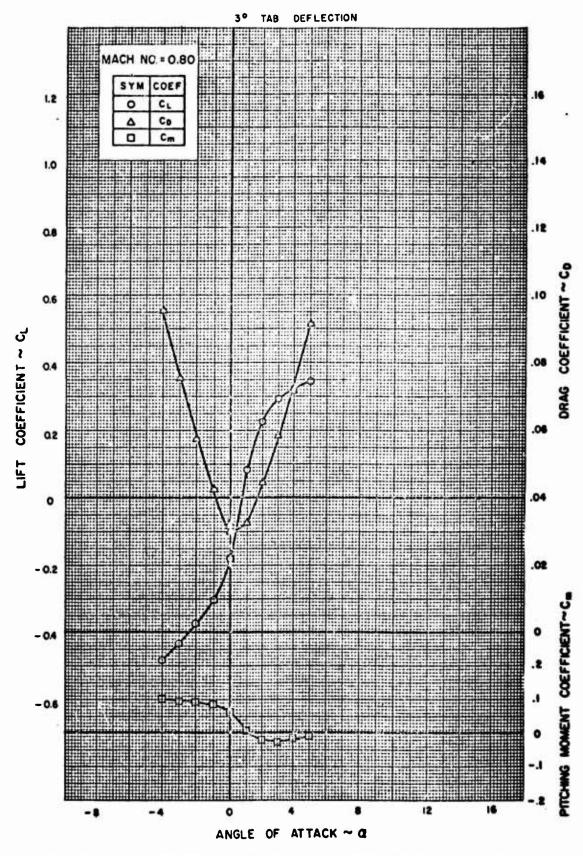


FIGURE 46. VARIATION OF FORCE COEFFICIENTS WITH ANGLE OF ATTACK

APPENDIX I

FORCE AND MOMENT COEFFICIENTS

SUPPLEMENTARY DATA

<u>M</u>	RUN	<u>a</u>	<u>C</u> L	c_D	_C _m
. 3	2	16	1.073	. 2255	102
. 3		18	-955	. 2834	113
. 3	2	19	. 992	. 3193	117
. 3	2	19	. 992	. 3193	117
. 3	2	20	. 965	. 3456	120
. 3	$\overline{2}$	21	. 930	. 3656	118
. 3 . 3	2	22	. 890	. 3818	116
. 3	2	24	. 853	. 4253	131
. 3	2	26	. 923	. 4936	170
. 3	2 2 2 2 2 2 2 2 2	28	1.023	. 5846	216
. 4	3	15	1.095	. 2109	071
. 4		16	1.079	. 2438	097
. 4	3 3 3 3 3 3 3	17	1.033	. 2757	111
. 4	3	18	. 986	. 2978	118
. 4	. 3	.19	. 939	. 3095	112
. 4	3	20	. 888	. 3292	113
. 4	3	22	. 844	. 8617	113
. 4	3	24	. 861	. 4189	133
. 4	3	26	1.003	.5332	173
. 4	3	28	1.055	. 59 29	190
_		12	1 014	1674	057
. 5	4	13	1.014	. 1674 . 2014	069
5	4	14	1.017	. 2316	084
. 5	4	15	1.012 .996	. 2594	095
.5	4	16		. 2875	106
.5	4	17 18	. 982 . 968	. 3136	118
. 5	4	20	. 909	. 3481	119
. 5		22	. 877	. 3857	129
. 5	4		. 994	. 4667	171
. 5	4	24	. 774	. 4007	1/1

M	RUN	<u>a</u> _	CL	CD	C _m
.6	20	12	. 95 0	. 1860	072
.6	20	13	. 982	. 2352	085
. 6	20	14	.998	. 2398	095
.6	20	15	1.006	. 2644	103
.6	20	16	.997	. 2915	115
. 65	8	12	. 916	. 2030	091
. 65	8	13	. 955	. 2308	103
.65	8	14	. 971	. 2545	107
. 65	8	15	1.005	. 2824	116
. 65	8	16	1.011	. 3080	133
. 65	8	17	1 035	. 3247	138
. 65	8	18	1.048	. 3359	145
.65	8	19	1.052	. 3492	156
. 65	8	20	1.051	. 3588	163
. 7	9	11	. 907	. 1934	090
. 7	9	12	. 918	. 2180	103
. 7	9	13	. 927	. 2434	- 116
.7	9	14	. 965	. 2633	122
.7	9	15	1.019	. 2845	148
.7	9	16	1.111	. 3047	167
			ree Tab De		
. 4	29	16	1.025	. 2386	- 086
.5	25	14	. 968	. 1945	048
.5	25	16	. 953	. 2575	- 078
.6	26	14	.928	. 2218	068
.6	26	16	. 942	. 2802	092
. 7	27	12	. 864	. 2087	075
. 7	27	14	. 883	. 2583	193
. 7	27	16	1.024	. 3039	145

APPENDIX II

TABULATED PRESSURE COEFFICIENTS

Pressure measurements-trailing edge tab not deflected.

Run No.	Nominal Mach No.	Angle of Attack Range, Degrees	Page No.	Related Fig. Nos.
2	0. 30	-4 to 26	58	5,6
3	0.40	-4 to 28	61	7,8
4	0.50	-4 to 24	64	9, 10
20	0.60	-4 to 16	68	11,12
8	0.65	-4 to 20	70	13,14
9	0.70	-4 to 16	74	15, 16
18	0.75	-4 to 10	77	17, 18
19	0.80	-4 to 5	80	19, 20

Pressure measurements-trailing edge tab deflected.

Run No.	Nominal Mach No.	Angle of Attack Range, Degrees	Page No.	Related Fig. Nos.
30	0. 30	-2 to 16	83	21, 22
29	0. 40	-4 to 16	84	23, 24
25	0.50	-2 to 16	86	25, 26
26	0.60	-2 to 16	88	27, 28
27	0.70	-2 to 16	90	29, 30
28	0.80	-4 to 5	91	31, 32

	30	2 1 0 30	RUN 2 MU 0.3	A S N D	6.	ACN 2	2 4 0 0 30	S S	3	S S	1	S S	
	₹Σ •	0 m	•30		0.301	Q Σ <	0.301	⊋ ₹ Σ •	2.0	Α Σ «	0.301	₹×.	90
	4 0 0	126.1 1988.0	126. 1988.	600	• • •	283	126.1				9 0	.88	126.1
×						9			0	ΰ		Ü	0
1 ,000		00	. 93	3	9.21		6	•			530		320
•008		26	.67	00	50	o.	1	•	10		-4	8	1-4
•017	<u>٩</u>	02	.37	9	0 6	0	4	0	3	0	7	50	3
040	٠ -	38	0000	60	22	0	2	0	00 -		p-4 0		4
000	_	m u	0.74	9	10	a 1	2	30	\$ 0		4 6	0 1	-4 C
2 6		424			120	0 0	7 0	0 0	630	9 4	823	1 1	130
168		10	0,26	0.0	79	0	0	0	11	0	759	0	973
.233	_	2	.30	-	98	0	00		5	9	1		3
335	•	0	*23	0	80	-	0		-	0	0		0
• 500	_	3	13		19		2	0	0		3	•	-
•625	•	18	· 13	00	87		4	3	8	•	-		5
• 169	9	0	.01	0	16		S		2	•	0		2
• 915	0	0	0.05	0	99	•	4		8	•	2		n
096	0 0	14	0.18	0 0	23	•	V)		-	•	3	•	N
800	-	12	0.45	500	ω ·	0	00 1	9	N		9 .	•	5
100	P 9	7	00/4		177	0	3 6		N	9	-	•	7 4 7
040	7	24	0 0	7 -	0	3 6	0 -	3 6	Vr		20		\$ 4
060	•	4	0.75	100		. 4	10		4 15		1 10		1 4
.130	9	46	.67	6	33	0	-	0	1		0		141
.168	9	47	-	8	60	•	5		1		2		-
.233	9	44	55	1.	38	•	-	•	-4		0		0
• 335	•	33	2	5	57	•	3	•	0		2		-
• 500	•	23	.31	3	30	•	3		9	•	2		0
•625	°	18	.21	.2	20	•	3	ċ	9		3		1
• 769	?	0	-0.092		98	0.0-	3		~	0	080	•	0
.915		S	0.05	0	14		3	•	169	•	2		0
0960		4	7	•	4.7		u		•		u	3	a

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	0.30	301	0.30	0.30	0.30	0.30	0.30
	8.0	10.06	11.0	12.0	13.0	14.0	15.0
	0 126.	126.1	126.	126.	126.	126.	126.
	0 1988.	1988.0	1988	1988.	1987.	1987.	1987.
	<u>გ</u>	8		a)	٥	a)	ā
00	.41	2.75	39	96	04	43	225
2 .008 U	Ü	-4.907	5	-6.160		-6.660	\ œ
•017	.18	4.34	•05	•65	6.13	6.17	5.59
070	.41	66.	3.29	.55	•65	.71	66.
• 065	1.97	.32	• 55	•74	•76	.83	2.98
060	.71	.97	•15	•30	.32	.38	647
•130	1.36	1.49	•68	•80	•77	.86	• 94
•168	1.17	1.31	74.	.52	14.	•57	• 59
9 .233	96.	• 02	•13	•24	• 16	• 28	.24
.33	0.71	0.71	.80	0.89	9	90	-0.867
1 .500	0.46	0.41	940	•53	• 45	0.53	.52
2790 2	0.30	•20	0.27	0.34	0.25	•35	• 30
2010	6 7 4 3	0.02	01.	•17	• 04	0.19	0.14
4. 915	0.0	•17	60	8	•12	10.	00
0960	•13	•19	•11	40.	• 16	•03	00
8000	66.	160	.77	•62	•63	•48	• 29
1100 /	96	95	66.	91	.97	• 63	• 95
040. 8	11.	.97	• 95	91	• 95	•92	66.
6900 6	.63	88	86	.81	•84	.82	.88
060 0	849	• 73	17.	.67	•72	• 70	.79
1 • 130	.37	999	990	•52	•62	•59	68
2 .168	• 30	• 52	.52	940	• 50	848	.56
3 .233	• 20	•39	040	•33	•39	.34	45
4 • 335	•19	• 35	.37	.29	.32	.29	37
. 606.	91.	•30	.31	•17	• 20	.20	.26
6200	9!	12.	• 22	0.07	•11	90	13
107	1/1	87.	170	•12	• 14	.12	15
CT6. 8	07.	930	.28	•13	.14	919	15

		MCN MCN					
	U 16.	AU 17.	18.	U 19.	20.	21.	22.
	0.30	M 0.30	0.30	0.30	0.30	0.30	0.30
	16.0	A 17.0	18.0	19.0	20.0	21.0	22.0
	0 128.	00 128•	129.	0 130.	130	130	130.
	0 1985.	P0 1985.	1984.	0 i 383.	1983.	1983.	1983.
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00	.87	.79	31	•89	16.0	•98	00
•008	.71	0.62	199	0.71	.72	•73	.72
.017	.76	.62	99	.71	• 70	7	72
040	.70	0.63	•66	0.70	0.68	.70	0.68
• 065	• 70	0.64	.66	.67	•68	• 70	•69
060	.71	0.65	.67	•68	•69	69•	.68
7 •130 U	-0.722	-0.666	-0.653	-0.681	-0.707	-0.700	-0.697
.168	19.	• 64	99•	• 70	•68	• 70	0
9 .233	.67	0.68	• 70	•71	• 70	•71	•72
0 .335	69	99.0	69.	•73	• 73	•73	• 76
1 .500	•72	•73	•72	• 75	• 76	•77	• 79
2 .625	.73	0.74	0.74	•81	.81	•84	.83
9 . 769	69	0.73	0.77	•84	0.84	•86	• 85
4 .715	\$0.	0.62	0.69	0.83	0.84	.87	888
0960.6	4 8	0.59	• 68	•85	.84	84	•87
9000 9	88	.85	.83	•84	• 84	•82	.83
7 .017	98	96	• 94	16.	.97	96.	96.
8 .040	660	• 95	• 92	• 95	40.	• 95	• 62
9 .065	48	80	• 78	.81	• 79	89	.82
060	.75	20	8690	69.	•68		8
1 .130	090	• 54	• 55	• 54	• 52	• 53	.52
2 • 168	.51	940	77.	•43	.41	•43	444
3 .233	•39	• 34	• 30	•30	• 28	• 28	•29
4 .335	• 28	•23	• 20	•16	.13	•16	•16
2 .500	• 16	60.	.0.	00.	.01	•01	.01
9 • 625	600	0.02	0.01	•07	· 09	.12	.11
1 . 769	0.02	60.03	• 07	•15	• 19	.21	•19
8 .915	00	•10	• 14	•24	• 28	.31	0
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É 3	0 0	MU 0.30	m e	4		MU 00.40	4
I	0.30	0.30	0.3	0	0.40	0 • 0	0.4
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ŏ	130.	132.	12	213	213.	213.	21
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	9	a		a	٥	ď	9
_	00	1.09	.97	01	90	.41	01
_	.76	0.83	.25	•28	.71	.95	29
•	•76	.81	.08	90.0	.39	.72	•03
	.74	0.80	34	36	.02	33	35
	.74	•79	•39	•38	.11	.15	.39
	.74	0.80	.41	0.45	.21	0.04	.43
	.74	6	.54	•43	•28	•02	.37
_	.75	•79	•39	.43	0.25	.08	38
_	•77	.81	• 38	.40	.27	.12	39
•	• 79	.80	•30	.32	•22	• 10	9
•	• 19	.82	•23	3	• 21	•12	20
_	-0.834	0	•	0	0		0
•	82	0.84	• 05	•04	0.0	8	.03
•	4 00	.81	~	90	• 10	0.113	60.
•	9 20	8	• 16	• 18	•17	• 19	• 19
	.81	•72	• 15	• 15	0	• 45	• 14
	• 95	.97	.16	•17	980	• 59	-0.209
	46.	•95	36	•38	.84		2
	.83	.85		-0.461	-0.934	•23	-0.493
	69.	•76	940	144	• 79	•13	.50
	.54	999	45	•48	0.74	66.0	64.
	.45	.53	.41	.42	• 65	.85	440
	90	•40	41	•45	.59	•75	.42
	.18	•31	.32	.33	• 46	• 58	.33
•	8	•10	•23	•23	• 32	•39	~
	.11	0.05		-0.169	•22		0.18
_	23	•12	• 03	0.03	0.08	• 11	• 05
_	.33	0.27	• 09	60 •	•07	90•	•08

	4.	12.0	04.	2.0	3	92.	۵	C	984	0	9	7	536	.9	-	4	a	~	ď	O .	œ	G	4	ø	2	~	658	~	2	~	~	126	9	660	N	•
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3 34	4	10.0	.40	0.0	4.	• 46		4	153	84	02	44	10	5	43	17	82	52	34	15	03	03	90	98	88	72	59	46	37	26	20	13	0	12	15	,
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	4	0.8	40	8.0	•	94.	<u>.</u>	7	653	47	19	6	4		~	0.6	9	64	35	9	02	0	66	Ø	75	~	43	30	54	4	2	9	04	8	15	
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		0.9	9	0.9	•	95.		20	441	35	0	1-	(1		98	83	59	35	22	9	12	20	98	83	58	38	7	14	11	02	00	00	02	05	12	
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3 3	4.0	4	0.40	4.0	213.	1895.	a	56	1.226	.39	.37	.17	60 •	0.88	0.80	0.71	0.52	0.34	0.25	0.10	• 08	• 15	.91	• 65	• 32	•13	• 04	0.03	0.07	0.12	0.10	0.07	0.08	• 05	.12	1
RUN	₹	¥	Σ	4	8	8 -					•	-		-	-	1		-		<u> </u>								1	_	-	-	.1	-			_
8 3 3	4	2.0	40	0	13.	5		96	0.344	49.	.83	.75	.75	79.	.59	.56	.43	•30	• 19	60	080	• 16	19.	• 28	03	• 16	•22	• 26	• 26	•29	.22	9	•13	• 03	• 00	•
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							-	0	.008 U	~	07	65	060	30	89	33	35	00	25	69	5	09	80	17	40	65	06	30	89	33	35	00	52	69	2	•
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	P0	86.7		82.	0	84.	P 0	81.4	0	79.	0 0	95.	0	83.
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O	-1-	24	0	87	•	•	•	~	1	32		(c)		
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040	0	97	c	S		C	0	œ	•	92	•	8	0	-
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- TABULATIC	4 5	0.5	9.	M 0.503	0.6	315.	1781.	و	0.75	3.39	•73	3.50	2.97	2.26	1.60	1.34	1.08	0.79	0.48	0.32	0.16	00•	•05	96.	96•	.81	.61	• 50	•37	•28	.18	•12	• 06	•04	• 08	0.137	•24
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								χ.	0	900	.017	040	• 065	060	.130	.168	•233	• 335	• 500	•625	• 169	•915	096	•008	•017	040	• 065	060	•130	.168	•233	• 335	• 500	• 625	• 169	.91	.360
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90	1.28	• 34	1,41	•24	.77	• 75	90
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40	• 05	• 07	• 03	•86		~	89
65	• 06	• 05	00	• 78	.67	.72	85
06	• 06	• 03	.97	.77	999	2	85
30	• 08	.01	97	•78	. 58	.72	80
.168 U	-1.008	-0.991	-0.926	-0.748		-0.732	-0.851
33	96	.93	.87	.74	• 66	.73	986
35	.86	.88	.84	• 75	•68	1	87
00	• 75	.78	6	•79	.72	S	88
25	0.68	0.72	.75	•80	• 75	•76	90
69	99	• 65	.70	• 78	.77	• 79	90
15	• 50	• 55	09•	•70	•75	•79	87
09	• 42	•51	.57	99.	.73	•79	86
90	• 98	66.	66.	66.	66.	.93	888
11	5	9	0.961	0960	95	96	95
40	.89	•91	.92	.92	96.	.98	98
69	.74	•76	.77	.77	.81	.85	16
90	.61	•64	•64	•65	•70	•74	80
30	• 48	• 50	.51	.52	• 56	• 59	68
68	• 39	•45	•43	•43	74.	640	59
33	•27	.27	•29	•30	•33	5	44
35	.17	•17	.18	•18	.21	.21	30
00	• 05	• 06	• 06	•05	90.	•05	112
25	00.	• 01	•02	•02	•03	40.	8
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20 27	9.0	9	.61	3.0	434.4	46.	ē	124	75		•03	96.	.94	•03	.92	•91	.88	.82	•77	• 68	• 56	.50	•94	96	•83	•65	.53	•39	•31	.18	.08	.01	• 05	€ U 8	10
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20 27	•	2.	.61	2.0	432.3	48.	و	18	66	1.797	.38	4	_	4	.12	S	96	L-	•67	• 56	•46	•42	•94	16.	81	•61	640	• 35	• 28	.15	90.	00.	• 05	•07	90.
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20 27	9	ä	•61	1.0	430.1	51.	و	, [71.		.79	.43	.35	.41	1.1	• 05	.91	.72	•61	. 51	040	•37	70.	96.	.77	•58	949	• 32	.25	•13	•04	00.	.05	•06	*0
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20 272	9.	10.	• 60	0.0	429.1	52.		•05	12		•16	.80	•62	.72	•32	• 15	•92	•65	.52	• 40	•31	.27	*6	660	•75	• 55	• 43	•29	•23	•10	•04	000	•04	•03	00
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UN 20 27	9.0	8	09.0	8.0	10 424.8	0 1657.	و	. 0	98	-2.279	.51	.59	640	•16	•76	• 30	.77	647	.33	•17	• 03	• 02	76.	96.	69.	640	• 38	• 25	.18	•07	•01	00.	00.	•02	•10
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20 20 20 20	e S	AU	0		00 42	16	و	.33	.68	-2.037	2.27	.42	2.37	.83	1.56	0.88	0.10	649	0.34	0.16	•03	•10	96.	.88	• 57	•36	•25	• 14	• 08	0.01	• 04	0.03	• 03	• 02	.12
20 269	09.0	0.4	0.603	*0	422.6	60.5		.68	.05	1.444	.77	.77	.57	• 10	•03	• 91	• 65	• 45	•31	• 14	• 02	• 13	• 62	.68	• 35	• 16	90.	40.	90.	• 15	• 14	• 10	•01	00	•12
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	U 14.	15.	U .16.	• : • :	0	·	-2.
	0.61	0.61	0.61	9•0	9•0	0.65	0.65
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	0 1644.	1643	0 1642	00	PO 1590.5	0 1590	1590
×	م	9					a)
00.	0.28	0.34	43	•06	• 0.8	8O.	10.
008	: 39	1.19	.28	•29	• 30	.53	. 1.2
•017	•07	1-4	20	.06	90.0	-17	. 7.
040	0.87	0.81	96	.43	• 45	•22	3.
• 065	.87	0.82	63.	• 50	0.54	• 34	4.1.
060	88	0.84	.87	• 55	0.61	• 43	.24
7 •130 U	-0.936		-0.820	-0.639	O	-0.534	-0.370
•168	.87	0	2	.52	0.58	45	.31
•233	.83	-0-	. 82	0.51	0.55	0.45	0.33
.335	•83	0	• 79	040	• 42	•36	• 28
. 500	.82	18.0	.81	0.32	• 29	.27	• 20
629	0.81	0.82	.83	123	.23	• 20	91.
• 769	0.75	80	0.83	60	0.08	0.	0.04
\$16	0.64	0.72	• 75	• 05	• 08	•07	•00
096	• 58	99.0	• 70	•17	• 19	• 18	• 20
• 008	96.	*6°	• 94	•24	• 32	•04	•24
•017	S	6.	46	• 14	90.0	•36	•68
040	• 86	. 88	• 90	•39	• 34	19.	.89
• 065	• 68	• 70	•71	.52	640	.74	•03
060	• 55	.58	•61	. 55	.53	• 75	00.
•130	.41	.43	946	•59	.58	11	16.
• 168	.34	• 36	•38	.53	0.53	.68	.83
•233	• 20	•22	•23	.53	.52	69.0	0.74
• 335	60.	.10	.12	642	07.	9	•56
• 500	• 01	•01	• 02	•30	0.28	• 35	•38
•625	0.07	0.07	0.08	.21	0.18	•22	• 54
• 169	• 11	0.12	•13	•07	• 02	•08	60.0-
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8 13	9	4.0	65	0	75.	6		ì	٥	• 84	• 54	•61	• 73	.72	.51	•70	96.	.63	• 45	• 33	• 16	•03	•12	• 93	99.	•34	•13	0.029	.08	•11	•20	•19	•16	•12	4	700
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8 13	9	3.0	65	0	74.	•		֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	• 0 1	• 59	.97	•37	.51	9		3	.86	•63	.45	• 30	• 13	• 03	•15	.85	• 52	•23	•03	990•	• 16	• 18	.25	.21	• 16	11.	•02	01.
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8 13	9	0.4-	•65	0	75.	89.		֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֡֓֓֓֓֡֓֡֓֡֓	0.0	• 95	• 70	•31	•13	• 02	0.114	.12	.17	•16	•14	•13	• 05	•00	•20	•86	•30	647	• 68	1.717	.74	•67	•79	• 65	• 45	• 30	•13	20.
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17	1.61	1.73	.82	.81	1.86	•	9	•	4
6 0	1.88	.98	• 05	•04	• 98	-17		•	144
0 59C	-2.032	-2.127	-2.098	-2.077	-1.859	-1-	583	•	268
06	2.02	2.10	66.	96.	.71	-1•	S	•	9
30	1,91	• 05	6	.83	8	-1-			8
80	2.03	2.10	.55	.52	.33	-1-	9	•	3
33	1.88	1.58	•28	•27	• 15	-1.	9	•	5
35	.72	0.92	00•	66.	67	0	3	•	∞
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52	.31	0.32	• 46	949	.51	•	-1	•	n
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08	• 95	• 94	• 94	• 94	• 93	•	3	•	B
11	. 85	.89	• 92	.92	• 95	•	-1	•	9
64	. 54	• 59	•63	•63	•67	•	-	•	4
65	• 33	040	43	43	• 48	•	2	•	4
90	•22	•28	.32	.32	.36	•	0	•	2
30	•11	•15	•19	•19	•23	•	9		œ
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33	•04	0.00	.01	010	40.	•	9	•	0
35	•06	• 04	0.04	•04	.01	•	-		0
00	•06	90.0	•06	900	.05		9	•	9
25	•04	90.0	0.07	•07	.08	•	0	•	0
69	• 03	0.00	03	•04	90.	ô	160	•	-
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	MU 0.65	MU 0.65	MU 0.65	MU 0.65	MU 0.65	MU 0.65	MU 0.65
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00	.08	0.01	08	16	• 26	-0.365	43
€008	S	63	.73	.72	69	76	19.
.017	1.72	1.58	.63	.77	1.80	1.89	.59
040	•21	1.26	60	93	44.	1.55	040
• 065	1.08	1.15	.02	.88	• 42	•54	•36
060	1.04	1.12	00.	.87	.43	• 55	.34
• 130	1.05	1.05	.97	0.88	1.24	2	•33
• 168	96.0	1.05	96.	•82	•41	•45	•18
• 233	0.92	1.00	0.91	0.86	1.31	•27	1.12
• 335	87	0.91	0.85	0.81	1.01	1.02	0.97
• 500	83	0.81	0.80	0.81	0.83	.87	0.89
624.	77	978	81	0.83	984	9880	0.00
000		7.0	71.0	1000	0000		76.0
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040	77.	.81	83	.86	9	92	46
_	0.588	0.627	0.657	0.691	0.742	0.759	0.786
060.	.46	.50	.53	•56	•62	•63	99
•130	.32	• 35	•39	.42	.47	640	.52
• 168	• 25	•27	•30	•33	• 38	040	•43
•233	• 10	•13	•16	•19	•23	•26	.27
• 335	• 05	• 03	•06	•08	.11	.13	.15
• 500	• 05	0.04	•04	•02	0	80	•01
• 625	11	0.10	0.11	17.	•00	60.	•00
• 169	•12	•13	S	• 16	• 15	16	~
.915	• 13	0.15	• 18	•20	• 20	•22	•23
040	0	(

	0		S	S	KON V LOS		Ġ	V
	MU 0.65)	.	5	0	0	0.7	0
	19	20.	0		AU -1.0	AU -2.0	•	0
	9.0	0.67	M 0.653	·	0.10	0.70	0.10	3
	19.	20.0	•0	•	-1.0	-2.0	-3.0	4
	498	•664	4	0 527.	0 527.	527.	528.	6
	1559	1558.	0 1590.	0 15	0 1521.	1521	1520.	
× 4		ď	ď		9	9	8	
00. 1	.80	9	•03	.11	•10	40.	96	_
•008	•79	15	.36	.36	•56	•73	84	
•017	•73	13	00	0.	.21	.41	56	
070	64	4	•38	45	.21	00000	115	
•065	94.	45	77	•55	.33	.15	8	
060	949	45	.51	•65	.43	•26	112	
.130	64.	36	67	.70	.54	04.	25	
•168	40	40	.48	63	74.	.33	23	
.233	39	32	940	2	.48	-0.374	28	
0 .335	.28	20	•33	642	•38	.31	25	_
1 .500	.23	7	.22	.31	.27	•23	13	
2 .625	.24		•15	.23	•20	.18	115	
3 .769	.25	7	•02	90.	•06	•05	10	
4 .915	.24	7	•13	60.	•00	O	10	
2 .960	.23	7	•23	•20	•20	.21	21	
900. 9	.74	9	35	.34	.10	4	39	
17 .017 L	0.774	0.937	60000	-0.053	-0.322		-0.818	_
8 .040	• 64	6	27	•34	•59	0.82	02	
6 .065	.48	80	.41	.52	•79	1.07	127	
060. 0	.37	69	.45	.58	.83	.11	29	
1 .130	.21	53	.50	99.	•95	•15	38	
2 .168	.13	44	44.	.59	.77	•13	38	
3 .233	.02	.2	.45	• 60	.74	.93	42	
4 • 335	.15	12	.34	94.	•54	0.58	99	_
2 .500	.29	0	.22	.31	•36	.40	04	
6 .625	41	• 16	.12	• 20	.24	0.26	27	
7 .769	50	-0.265	00	90	90	60.0	10	
8 :915	2	50	.14	•11	.10	60.	80	_
096° 6	42		• 56	•22	• 50	•19	19	

9 160 RUN 9 161 RUN 9 162 RUN 9 0.70 MU 0.70 M						
RUN 9 157 RUN 9 156 RUN 9 160 RUN 9 161 RUN 9 162 RUN 9 163 RUN 9 164 RUN 9 164 RUN 9 164 RUN 9 164 RUN 9 165 RUN 9	9 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1514 CP 760 832	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	890010		100
Name	% X X X 4 8	2 017	777777			
AP X/C MU O-70	9 16 0 5 0 5 0 0 5 0 5 3 1 0	1516. 811 661 664	w w w w w w w w w w w w w w w w w w w	120017	1100011	257
RUN 9 157 RUN 9 156 RUN 9 160 RUN 9 161 RUN 9 160 AU 0.70 MU	% X X 	2 097	777777	9990000	°°°°°°°°°	990
AP X/C MU AU AU AU AU AU AU AU AU AU	9 16 0.7 0.70 4.0 529	1518• CP •894 •529	8 4 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	60 H C C C C C C C C C C C C C C C C C C		22.2
AP X/C AU 0.70 MU 0.7	233×48					
AP X/C AU 0.70 MU 0.70	9 161 0.70 3.0 0.705 3.04 528.9	1520. CP 980 375		E 540 48 8	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	404
AP X/C CP AU 0.70 MU 0		000	777777	9990000	0000000	990
AP X/C AU 0.70 MU 0.70 AU 0.70	9 160 0 70 2 0 0 704 2 03 527 8	1521.5 CP .061 .151	6 4 4 4 4 6 6			200
AP X/C AUN 9 157 RUN 9 157 NUN 9 158		<u> </u>	9777779	9990000		990
A NUN A NO	9.1 0.0 52.4	1521 CP 102 104	6 8 8 8 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	00000000000000000000000000000000000000		91.05
A NUN		2 709	777777	7770000	7777777	770
	9 15 0 - 7 0 - 70 529	1518. P 878 924 661	2215	7660144	144455000	1126
$\begin{array}{c} A & 1 & 1 & 2 & 2 & 3 & 3 & 4 & 4 & 4 & 4 & 4 & 4 & 4 & 4$	13000	•	0000000	0000000		000
4 1 2 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4						
4-10-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4		×885	900 H H B B B B B B B B B B B B B B B B B	922910	4 9 9 5 4 5 6 6 9	91 91
		4	* 10 0 7 0 0 0	100400	800HN845	w~ w

ON 9 16	RUN 9 166	9 16	91 6 NO	91 6	N 9 17	N 9 17
MU 0.70	04.0 O*40	MU 0.70	MU 0.70	MU 0.70	MU 0.70	MU 0.70
	A C C C C C C C C C C C C C C C C C C C	0.71	0.71	0.71	0.72	450
7.0	8.06	0.6	1001	11.0	12.0	13.0
0 535.	00 537.1	539	0 541.	543	545	548
0 1511.	P0 1509.2	1506	0 1503.	1501	1498.	1494
	9	a	ą	9	a)	a)
•65	.58	.50	43	.37	.31	•25
c	-		-1.292	-1.383		-1.503
1.29	.37	44.	649	.51	.53	.58
.55	.62	•64	58	1.45	•22	•16
1.69	1.72	4	17.	.37	40.	.87
1.66	1.71	~	39	.30	000	•84
. 58	.70	.53	33	.23	03	.86
.72	1.57	-1.294	25	80·	.89	.81
67	1.27	•00	70	96.	0.85	0.80
•12	• 62	• 93	83	•85	85	80
4	0.75	œ	8.	.82	.82	.81
• 35	0.55	99•	• 76	• 79	•82	•83
• 18	0.37	• 53	67	.74	•80	•84
900	0.24	14.	56	• 64	3	.80
0.	• 20	• 36	.51	• 60	69.	•78
96.	• 95	•94	93	.92	.92	•92
4		0.922	95	96.	066.0	30
.53	.57	•63	67	•71	47.	.77
• 34	•37	•43	949	.52	•55	.57
•23	•26	2	36	949	.43	.45
600	• 12	• 18	21	• 25	•28	.31
40.	• 07	• 12	14	.18	•21	.24
90.	• 05	00•	0	•04	•07	.08
01.	0.10	•07	90	•04	•05	001
• 11	0.13		11	• 11	•10	•10
•10	0.13	•13	0.15	• 15	•15	.18
•04	60.		14	• 16	8	.21
• 02	0.00	• 05	10	-	1	0.20
. 18	-	5	0	00	C	ď

RUN 18 229		97	0 0 0	0.664	1453		600	0.727	040	000	.16	8	4	0	S	96.0	0.27	2 6	0.11	•22	5	•39	•65	9	96.	• 05	•07	•17	.18	64.0	.18	09000	11
228		201	00,700	582.1	1454.9	9	.12	999	• 26	•15	.31	.41	999	.52	.57	•43	0.29	770	0.11	•22	.17	•22	.51	•76	.81	•91	96.	40.	.03	.31	.21	10.063	71.
RUN 18 227	3		0	583	14		•13	0.43	• 06	• 36	.51	•61	.74	• 78	0.79	649	0.33	200	0.10	•21	•37	010	•33	.54	.62	•79	.81	.81	. 48	• 34	0.22	990-0-	71
RUN 9 175			0	527	15	<u>a</u>	•10	.34	•03	14.	•57	99•	•86	•65	0.62	•47	0.34	000	07	.19	.34	•03	•34	.52	0.58	999	•59	09.0	0.46	•32	•20	-0.061	1
3 RUN 9 174			2/ •0	553	487		00	58	.72	•28	•27	.25	•20	•17	1.07	• 05	96 0	000	0.98	96.	.91	•93	.88	.70	.58	.43	.34	.19	.05	.05	0.15	-0-215	3300
17		10	15.0	551	1490		.10	1.48	• 43	• 99	96.	• 95	.92	0.93	0.92	0.00	90	96.0	0.93	0.00	.91	*6 •	•85	.67	• 55	040	.31	.16	• 04	90.0	0.16	-0.220	1
2			14-0	540	0 1492.		.18	849	.17	.86	81	.81	.82	.79	.78	89	8 9	80	.86	.83	.91	96.	80	.62	640	35	.27	11	00	60.	-17	10.220	,
						-	00	•008	.017	040	• 065	060.	130	.168	•233	• 335	0000	.769	.915	096	•008	•017	•040	• 065	060	.130	.168	.233	• 335	• 500	•625	- 107 -	

. .

18 236	_	4	92	0	•	•64		0.5	18	55	91	14	13	14	23	.31	.32		.54	.18	•02	.08	• 85	.55	.22	•03	.08	•21	.22	.32	•29	•24	~	9	•106	2
RUN	₹	¥	Σ	<	8	8			9	9	P	ī	-	-1	-	7	ï	٥	9	Ŷ	0	0	0	0	0	<u> </u>	°	°	î	Ŷ	<u>٩</u>	Ŷ	î	٩	0	C
18	1	Ö	75	0	•	52.	9	-07	0.0	.43	.82	00.	.02	5	613	• 22	•25		•25	•07	•08	.17	.78	.45	• 13	• 02	• 16	•29	• 29	•38	•33	.24	•16	40.	•13	46
S C	₹	¥	Σ	<	00	P0			- i	1	7	- -	7	î	ī	7	7	<u>٩</u>	ነ _	<u>۲</u>	_	_	-			۲ 	የ 	ř	የ —	۲ -	۲ _	۲ _	የ _	?	0	_
RUN 18 234	0.1	2.	0.75	2.0	583	1453.	d	- 1 -	0.07	\$23	0.70	.87	• 90	90	.03	•13	•15	0	• 20	.08	· 10	•20	.67	.32	.01	.18	• 28	.42	• 39	.48	•37	•26	.17	•04	12	23
RUN 18 233	0.7	 	0.75	1.0	0 582.	0 1454.		13	.25	10	.54	69.0	0.71	78	• 88	000	• 30	-0.317	•23	•08	•10	•21	• 54	.14	0.16	•35	444	9.0	• 56	•63	643	•29	•19	•06	12	22
RUN 18 232	0.7	ċ	0.7		581.	1456	9	3	43	90	.36	.52	.61	.72	67.	.80	• 50	-0.337	.25	•00	•03	• 20	• 36	• 03	0.34	• 55	• 63	• 79	8.	.80	647	.34	.22	•07	0.113	. 23
RUN 18 231	0.7	-4-	0.76	0.4-	586.	1449.		00	89	09.	.21	.03	.08	.21	•23	.31	•29	-0.243	•20	• 00	•08	•19	0.25	0.65	85	1.09	1.15	1.23	1.25	• 34	1.28	69.	0.60	•24	0.00	0.5
N 18	0.0	U -3.	0.75	-3.0	0 584.	0 1452.	ď	10	81	.51	.12	0.04	0.17	0.32	0.30	0.37	0.32	-0.251	0.19	0.07	• 10	•21	0.12	0.54	•77	1.02	1.06	1.16	1.17	1.25	1.28	0.67	0.33	0.05	• 08	715
								Ċ	80	17	0	55	06	30	89	33	35	200 C	52	69	15	09	90	17	0	9 2	06	90	68	33	35	00	25	69	15	C

										•											
RUN 18 243 MU 0.75 AU 0.755 A 0.755 OO 581.1 PO 1456.3	CP - 12		0.51	.61	.77	0.50	0.35	96	•00	.37	•02	0.34	0000	700	.81	.82	64.0	0.34	17.	.12	22
RUN 18 242 MU 0.75 AU 10.0 M 0.778 A 10.04 O 603.6 PO 1424.5	CP 00.71		1.42	• 40	46	2	91	93	98		88	53	200	100	40	60	18	28	2 0	170	0
RUN 18 241 MU 0.75 AU 9.00 M 0.773 A 9.04 QO 598.7	CP 0.75		1.40	.40	44	0.92	48.	0.81	• 46	9	.85	.55	• 34	270	.02	• 12	0.19	0.27	0.25	12	00
RUN 18 240 MU 0.75 AU 8.0 M 0.769 A 8.04 QO 594.8	CP • 80		1.36	.38	1.39	.86	980	0.71	0.52	44.	.81	• 50	.31	079	010	•14	0.19	0.20	0.23	010	0.05
RUN 18 239 MU 0.75 AU 7.00 M 0.767 A 7.04 Q0 592.9 P0 1439.7	0.80	0 -	1.29	33	35	0.82	•76	0.62	040	20	•75	44.	• 23	02	0.07	0.19	.22	0.26	120	0.03	08
RUN 18 238 MU 0.75 AU 6.0 M 0.764 A 6.04 QO 589.9	CP 0.92	-0.753 -1.083	1.24	•27	1.35	0.85	275	0.53	0.27	0.20	69.	• 38	91.	0.07	0.10	0.22	•24	62.0	77.0	0.01	.13
RUN 18 237 MU 0.75 AU 5.0 M 0.762 A 5.04 Q0 588.0	CP 0.97		1.18	.21	1.31	1.02	0.73	0.38	• 10	0.92	.63	.31		0.13	0.16	0.27	• 26	97.0	0.0	0.00	119
	TAP X/C 1 .000	60.5	065	.130	.168	0 .335	1 .500	3 .769	4 .915	960	7 .017	8 .040		1 .130	2 .168	3 .233	4 • 335	0000	2700 0	8 .915	096. 6

	RUN 19 245	61 N	RUN 19 247	RUN 19 248	61 N	RUN 19 250	01 N
	0.8	00	0 1		X		D C
	•	71	•7-	• • • • • • • • • • • • • • • • • • • •			4 6
	0.8	0.81	19.0	18.0	78.0	0	79.0
	•	-1.0	2.0	-3.0	0.4-	•	1.0
	633	634.	636.	0 639.	641.	0 633	634.
	1380.	1378.	1376.	0 1371.	1369.	0 1380.	1378.
/× d							
00	5	4	-13	12	00	15	15
800°	640	5.9	•67	.74	.81	640	38
•017	• 15	•25	34	643	.50	.14	.02
070	.29	0.16	60.	.01	90.	.29	14.
• 065	.42	0.31	.23	.13	.07	645	.55
060	.50	0.42	.35	.26	61.	.50	.56
.130	.55	0.58	5¢	-0.464	040	.58	.68
.168	69.0	0.63	.51	14.	0.36	69.	77.
•233	•80	69.0	•63	.57	.52	.83	.88
0 -8335 U	-0.868	-0.784	-0.726	-0.647	-0.597	-0.866	-0.944
• 500	• 90	0.40	•68	• 56	.63	90	000
. 625	• 20	0.17	•20	•25	.32	.27	040
.769	0.	90.0	• 10	•16	•21	•05	120
.915	15	• 10	3	•01	900	• 13	03
. • 960	• 24	• 20	• 13	•07	•04	• 23	• 10
• 008	44	• 34	.25	• 10	•00	.43	• 54
•017	•04	0.03	•12	•23	0.30	•02	•17
000	0.23	0.32	040	.41	.53	•23	• 12
• 065	0.45	0.57	49.	• 70	• 16	• 45	.34
060	. 52	0.62	0		.82		• 42
•130	99.0	0.74	.80	.87	.92	•67	09.
• 168	0.7i	0.78	.84	•90	.95	.71	+9.
.233	.82	.89	4	66.	•03	.84	•72
. 135	0.86	96.0	.98	•04	.08	.87	.77
• 500	76.0	1.00	~	.59	99.	£6.	.71
•625	•31	94.0	.45	8	.53	•29	.15
• 169	00	0.32	•39	.45	.51	00.	.02
.915	.15	0.08	9	•37	649	.14	.14
070	•	(

RUN 19 256 RUN 19 257 RUN 19 25	AU 0. AU 1.0 AU 2.	M 0.810 M 0.811 M 0.81	A 00 A 1000 A 200	PO 1380.2 PO 1378.8 PO 1376.	a)	10159 1014	.491 0.389 0.30	•142 0•037 -0•04	.276 -0.379 -0.45	•427 -0.546 -0.63	•516 -0.563 -0.65	.753 -0.692 -0.72	0.708 0.154 -0.81	0.813 -0.877 -0.92	0.0880	78°01 70°01 08.6°	0.022 -0.280 -0.38	.139 0.031 -0.20	•736 0•105 -0•12	•452 0.548 0.62	.088 0.193 0.27	•224 -0.124 -0.04	•441 -0.337 -0.25	0.516 -0.425 -0.34	0.654 -0.595 -0.54	0.705 -0.638 -0.50	0-K19 -0-/13 -0-65	455 - 10 - 769 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	7190-1	610-0-	
N 19	. 5.	0.82	2.44	1365	9	•00	•03	•30	•66	•84	.88	0.93	66.0	1.08	1011	500	0.57	0.56	.51	.84	.53	.21	00	01.	0.26	0.28	0.40	-0.375	79	0.21	
RUN 19 254 MU 0.80	. 4.	0.81	0.4	0 1369.		.12	11	.23	•61	.78	.82	0.86	• 94	1.03	200	40.0	0.51	47	.41	.78	45	•14	90.	0.17	0.33	0.34	26.0		0.33	16	
RUN 19 253 MU 0.80	3.	0.81	3.0	1373	9	.13	.20	0.14	0.56	0.71	0.75	0.78	0.88	0.98	1003	100	0.46	0.37	0.29	.75	•36	• 05	0.15	0.26	6490	0.40	70.00	01990-	0.21	0.11	
RUN 19 252 MU 0.80	U 2.	0.81	2.00	0 1376.		.14	.29	0.05	640	•64	99.0	0.72	0.82	0.93	26.00	600	0.39	.21	•13	•62	•27	•03	0.24	0.34	66.00	04.	1000	+1/*0- -0.644	17	•07	
					×	00	900	.017	040	• 065	060	•130	•168	9 .233	0000	628	3 .769	4 .915	960 9	900 9	7 .017	070 8	6 • 065	0600	1 • 130	891. 2	0000	14 0.330 F	6 .625	49L L	

STN.		
E COEFFICIE 3UN 19 262 4U 0.80 NU 0.810 NU 0.810 NU 0.810 NU 0.810 NU 0.810 NU 0.810 NU 0.810	C	といっていかりここりこう
AUN 19 261 NU NU 0.80 NU 0.82 NU 0.822 NU 0.822 NU 0.822 NU 0.822 NU 0.822 NU 0.822 NU 0.823 NU NU 0.823 NU	00000000000000000000000000000000000000	000000000000000000000000000000000000000
- TABULATI RUN 19 260 MU 0.80 AU 4.0 M 0.818 A 4.02 O 641.3	U	
S-58 AIRFOIL RUN 19 259 MU 0.80 AU 3.0 AU 0.816 A 3.01 OO 639.4 PO 1371.9	00000000000000000000000000000000000000	400000 CUUUL
	X	

	N 30	RUN 30 366	RUN 30 367	RUN 30 368	36	370	
	0°3	0.3	0°3	0.3	0.3	0.30	0.3
	• •	-2-	° 0	2.	, 4.	0.9	8
	0.3	0.30	0.3	0.30	0.30	0.301	0.30
	•	-2.0	•	2.0	4.0	6.04	8.0
	0 126	126.	0 12	126.	126.	126.5	126.
	0 1994.	1994.	0 1994•	1994.	1994.	1994.6	1994.
-	و		9	9	9	ď	٠ م
Ò	95	.79	46	90	57	.23	3
80	20	63	29	31	13	2.21	48
11	.08	•39	40.	0.60	• 28	.16	.12
04	47	0.08	040	.85	3	1.93	54
65	640	0.19	14.	.77	.15	.52	96.
06	.51	.26	.46	77	1.03	.36	.73
30	.58	0.33	43	•63	.89	.12	F4
68	47	• 32	•43	•61	• 78	0.	2
33	640	0.33	•41	5.7	0.71	•86	-
35	.37	0.28	36	.43	.54	•64	77
00	.34	•27	.26	•33		.46	50
25	• 26	0.22	9	•24	5.7	•30	.36
69	60.	60.0	•05		.12	•16	•16
15	010	0.02	01	000	010	000	0.00
09	10	.11	• 14	.12	12.	000	•07
90	•03	99•	•04	.42	.77	.88	.91
017	• 39	76.0	.38	•06	.51	• 75	•89
04	.54	• 93	.58	0.18	• 16	77.	• 65
65	99.	• 93	69.	•37	.01	•22	.41
06	•64	.87	99.	-	900	.14	.30
130	•63	.82	64	•421	.15	00.	• 18
68	.57	.71	•59	.42	.21	.01	.15
33	• 55	• 65	8	540	• 26	•07	900
35	643	•53	.45	.33	1.8	90.	00.
00	.33	.41	.37	•28	0.18	.10	.02
25	.30	.31	.32	25	.18	0.13	900
69	•15	•20	.16	0.14	.07	0.04	00.00
915 1	-0.043	-0.056	890.0-	0	0	90000	0.031
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RUN 29 353 MU 0 460 AU -2.0 M 0 401 A -2.02	1901.	.83	• 70	140	00.	-0.118	0.40	0.26	0.29	• 23	• 20	0.16	40.	200	.0.	÷6.	•92	• 94	.87	.82	.71	•68	.53	•39	6.28	-0.161	0
0.00	1901 CP	.00	.33	8	S		0.46	0.43	14.0	• 32	•24	0.15	00	0.00	.08	27	940	• 54	• 55	• 56	.51	640	.41	•31	•25	-0°098	• 03
0.00	1994 CP	•93	• 19	• 08	144	-0.502	0,00	0.52	0.52	• 39	• 34	•27	1100	200	909	95.	.48	• 57	• 56	• 55	. 52	• 51	•43	• 33	0.23		• 02
MU 30 375 MU 0.30 AU 16.0 M 0.303 A 16.05	0 1993.	2.67	68	.85	.70		0.00	0.70	•73	• 74	• 75	•75	0.72		.65	.92	16.	• 77	•64	• 51	.41	•28	•17	•04	0.01	90.0	41.
RUN 30 374 MU 0.30 AU 14.0 M 0.302 A 14.07	1993.	•83	.15	• 41	•04	-2.976	1.05	1.66	1,30	• 95	• 58	0.39	•21		36	16.	. 88	• 83	•65	• 52	.42	• 32	•21	• 10	010	404	20.
MU 0.30 MU 0.30 AU 12.0 M 0.301 A 12.07	1994.	3.90	.12	5.59	3.72	-2.751	1.85	1.56	1.27	0.91	0.59	040	100	0.03	.56	.92	•86	•71	.57	5 7 7	• 38	•24	• 18	•11	• 02	• 02	70.
RUN 30 372 MU 0.30 AU 10.0 M 0.301 A 10.06	0 1994	2.60	4.79	.23	3,19	-2,389	19	2401	1,15	0.86	0.56	• 36	0.16	900	.82	.92	.77	• 62	24.	• 34	• 29	• 19	•12	• 02	00	• 03	• 03
	×	00	• 008	• 017	040	5 .065 U	130	.168	•233	•335	• 500	•625	. 697	.096	.008	•017	040	• 065	060	•130	.168	•233	• 335	• 500	•629	• 769	67.6

RUN 29 36	£	AU 10.	0 0 E	A 10.0	00 215	F0 1900.	9	. 96	00	65	.08	.43	•08	•64	643	1.17	0.85	0.55	0.35	-	9 6	0.916	98	.83	• 64	.52	•39	• 29	• 18	.12	•00	00	\$ C	
RUN 29 35	MU 0.40	8	0.40	8.0	214.	1901.	9	0	.61	.31	999	• 05	• 78	440	•24	1.03	0.76	0.51	.33	9 6		0.976	46	.71	.51	• 38	• 24	•16	900	40.	80.	•05	200	
UN 29 35	MU 0.40	•9 0	0.40	0.9	0 214.	0 1901.		-	2.27	2.26	.01	1.60	444	1.9	• 04	.91	9.46	• 46	•31	•	200	0.953	81	.50	•28	•17	• 05	• 05	• 05	90.	0.07	0.08	500	•
29 357	MU 0.40	4	0.40	4.0	214.	1901.	و	59	.15	1.33	•36	.17	1.07	0.91	0.80	•73	0.55	0.39	0.25	110	,	0.841	59	.25	•04	1000	0.13	•15	0.20	•16	0.15	•13	40.00	
UN 29 356	MU 0.40	U 2.	0.40	2.0	0 214.	0 1901.	و	.97	26	.58	.82	.75	~	•62	.59	0.54	0.42	0.30	0.20	0 0	200	0.541	20	.10	•26	.31	0.34	0.31	.35	0.28	0.22	0.20	500	
29 355	MU 0.40	0	4.0	0	214.	190	و	00	.32	0.01	.35	.40	77.0	0.43	0.42	040	0.31	0.23	0.16	0000	200	0.031	0.31	0.50	0.61	09.	0.57	0.54	0.52	0.42	0.32	0.26	000	
RUN 29 354	0 0	U -4.	0.40	14.0	0 214.	0 1901.		27	96	14	.32	15	• 05	11	60.0	.14	0.12	0.13	0.11		200	-1.614	78	1.52	1.34	1.22	1.07	0.92	0.83	0.65	0.45	30		
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RUN 25 306 MU 0.50 AU 0.502 M 0.502 A 0. QO 315.4 PO 1768.2	F 0 40	W 4 4 4 4 4 W	0000000	00000 4 W @ @ W W W O O 4 K	##O##O
RUN 25 305 MU 0.50 AU -2.0 M 0.502 A -2.02 OO 315.4 PO 1788.2	4 7 8 7	000000000000000000000000000000000000000	0000000	225	1000 1000 1000 1000 1000 1000 1000
RUN 25 304 MU 0.50 AU 0.50 M 0.502 A 0.502 PO 1788.2	CP 1.044 0.357 0.004	W 4 4 4 4 4 W	0000000	00000 4 W W W W W	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
RUN 29 364 MU 0.40 AU 0.401 M 0.401 A 0.400 QO 214.0	P 0 0 0 0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0000000	4 ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	0.000
RUN 29 363 MU 0640 AU 1660 M 06407 A 16604 QO 21967 PO 16956	\$ 0 00 ·	00000000 00000000		36672	0.251 0.058 0.028 -0.037 -0.085
RUN 29 362 MU 0.40 AU 14.0 M 0.405 A 14.06 QO 217.8	CP 1.19 1.38	1.18 1.15 1.12 1.01 0.97	10.479 10.5681 10.415 0.9565	34667	0000
RUN 29 361 MU 0.40 AU 12.0 M 0.402. A 12.07 Q0 215.0	CP 2.49 5.26 5.10	3.69 2.76 2.77 11.79 0.80	10.559 10.348 10.198 10.086 10.058 0.788	2 C C C C C C C C C C C C C C C C C C C	0000
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RUN 26 317	U -2.	09.0	-2.0	0 422.	0 1661.		6	78	4	•04	•07	•16	•25	S	56	7 :	-0-181	0.02	.11	25	•50	4	•07	•14	1.04	66.0	•84	• 78	0	•45	•29		90.
RUN 26 316	•	0.602	•	0 421.8	0 1662.6	ą	, 6	04	0	.37	.42	14.	• 50	0.45	0.45	0.50	16290	0.05	.11	•23	9	•21	• 45	• 58	0.61	0.64	• 58	• 56	4	• 32	• 22	-0.101	90.
RUN 25 315	0	0	0	315.	1788	٥	0	30	010	•39	0.42	.46	0.64	0.45	.41	0000	-0.274	90.0	.08	•22	.11	0.23	77.0	0.57	0.56	0.57	0.52	0.51	0.41	•29	0.21	60.	90.
RUN 25 314	16.	0.51	16.0	0 323	0 1778.		, a	1.040	28	0.98	96.0	.93	• 95	06 0	0.89	000	10.807	0.67	0.57	• 50	96.	16.	•88	• 72	19.	• 45	• 38	• 25	•13	03	0.05	60.	0.15
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RUN 27 333 MU 0.70 AU 6.00 M 0.708 A 6.06	1520. CP	0.76		1.64	0 0 N	•25	100.	.47	0000	19	0000
RUN 27 332 MU 0.70 AU 0.706 M 0.706 A 4.05	1523. CP 0.946	0.83	1.27	1.32		• 25	22	.28	0.02	23	100000000000000000000000000000000000000
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RUN 27 329 MU 5.70 AU -2.0 M 0.704 A -2.03	1525. CP	.47	.08 .18	0.36	0.27	• 14	0.26	.91	1.27	0.00	-0.300 -0.134 -0.056
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RUN 28 341 MU 0.80 AU -1.00 M 0.812 A -1.00 GC 635.4 PO 1376.8	CP .14	.30 .58 .61 .68	0000000		00000
RUN 28 340 MU 0.80 AU 0.811 A 0.811 00 634.5 P0 1378.2	CP 15 00 517 00 399	444 644 80 80 80	3404V401		200
RUN 27 339 MU 0.70 AU 0.704 A 0.529.3 PO 1525.8	0487	400004	0000000	400000000000000000000000000000000000000	1230
RUN 27 338 MU 0.70 AU 16.0 M 0.729 A 16.04 QO 554.8 PO 1491.5	0.03 11.55 1.33		0000000	~ ∞ ⊙ ~ ~ ∞ ⊙	23
RUN 27 337 MU 0.70 AU 14.0 M 0.725 A 14.04 OO 550.8	CP 10.53 10.53 10.63	444		0 0 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000
RUN 27 336 MU 0.70 AU 12.0 M 0.721 A 12.05 GO 546.7 PO 1502.5	00.00	1.14 1.09 1.09 0.11 0.87	0.000000000000000000000000000000000000	24 24 24 20 30 30	1222
RUN 27 335 MU 0.70 AU 10.0 M 0.716 A 10.05 O0 541.6 PO 1509.3	00.46 11.26 11.63	044408 004878	00000000000000000000000000000000000000	64 W140 64 9 W 0 B	100
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• 169	• 52	•	-0.003		
•915	04.	.51	.15		
096	30	-0.427	0.273		
•008	7	.84	• 42		
•017	5	0.544	0		
040	0.142		.22		
•065	0.07	00.	46		
060	-0.176	660.0-	-0.527		
•130	-0.346	-0.263	99		
•168	-0.350	-0.285	-0-719		
•233	-0.532	-0-471	8	•	
• 335	967.0-	-0.356	88		
• 500	-0.709	-0.689	9		
•629	-0.563	-0.685	-0.593		
•769		040	28		
•915	-0.072	-0-148	0		
070	700		1		